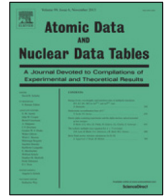




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Transition rates and radiative lifetimes of Ca I

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ABSTRACT

We tabulate spontaneous emission rates for all possible 811 electric-dipole-allowed transitions between the 75 lowest-energy states of Ca I. These involve the $4sns$ ($n = 4-8$), $4snp$ ($n = 4-7$), $4snd$ ($n = 3-6$), $4snf$ ($n = 4-6$), $3d^2$, $4p^2$, $3d4p$, and $4s5g$ electronic configurations. We compile the transition rates by carrying out *ab initio* relativistic calculations using the combined method of configuration interaction and many-body perturbation theory. The results are compared to the available literature values. The tabulated rates can be useful in various applications, such as optimizing laser cooling in magneto-optical traps, estimating various systematic effects in optical clocks and evaluating static or dynamic polarizabilities and long-range atom–atom interaction coefficients and related atomic properties.

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1. Introduction

Alkaline-earth atoms and divalent-like atoms (such as Yb and Hg) became a subject of interest to the cold atom community in the past decade. These atoms possess two valence electrons outside a tightly bound core and in the LS coupling scheme, the atomic states can be classified by being either singlet or triplet states. The availability of relatively wide spin-allowed and narrow spin-forbidden electric-dipole (E1) transitions enables stacking laser cooling on both types of transitions, with the spin-allowed transitions used for the initial rapid cooling and spin-forbidden transitions—for reaching much lower Doppler-limit temperatures. Moreover, the narrow inter-combination transitions, such as the $4s^2 \ ^1S_0 - 4s4p \ ^3P_1$ transition, can be used as an optical frequency Refs. [1,2]. The highly-forbidden $4s^2 \ ^1S_0 - 4s4p \ ^3P_0$ transition can be potentially used for an optical lattice clock scheme [3]. However, due to peculiarities of its electronic structure, Ca, unlike other alkaline-earth atoms, has a relatively short lifetime in conventional magneto-optical traps (MOT). To improve the MOT efficiency, several re-pumping schemes were proposed and demonstrated [4]. That work required reliable electric-dipole transition data for many transitions between the 75 lowest energy states of neutral Ca. Here, we compile the results of our computational work that served as a basis of the MOT performance analysis [4]. We anticipate that the tabulated data will be useful in multiple other contexts, such as estimating various systematic effects in optical clocks and computing static or dynamic polarizabilities and long-range inter-atomic interaction coefficients.

There have been a number of atomic-structure calculations for neutral calcium. The earlier work includes multi-configuration Hartree-Fock (MCHF) calculation [5] and semi-empirical model-potential calculations [6–9]. These computations provide oscillator strengths for spin-allowed transitions for levels up to $4s10s$, $4s9p$ and $4s6d$. Most of them are non-relativistic with very limited numbers of low-lying levels treated with *ab initio* relativistic methods. In particular, Fisher and Tachiev [10] reported energies and E1 transition rates for levels below $3d4p \ ^1F_3$. Porsev et al. [11] and Savukov and Johnson [12] computed the $4s^2 - 4s4p$, $4s4p - 3d4s$, and $4s4p - 4s5s$ transition rates using a combination of configuration-interaction (CI) and many-body perturbation theory (MBPT) (referred to as the CI+MBPT method). The CI+MBPT method results were in excellent agreement with high-precision experimental values. This fact partially motivated our use of the relativistic CI+MBPT method for the present work.

2. Computational details

The CI+MBPT method employs a systematic formalism that combines advantages of both configuration interaction (CI)

method and many-body perturbation theory (MBPT) [13]. This method has been used extensively for evaluation of atomic properties (see, e.g., review [14] for optical lattice clock applications and references therein). Relativistic effects are included exactly as the formalism starts from the Dirac equation and employs relativistic bi-spinor wave functions throughout the entire calculation. In our treatment, the CI model space is limited to excitations of the two valence electrons. Contributions involving virtual excitations of core orbitals are treated within the MBPT. In this approach, we first solve for the valence electron orbitals and energies in the field of core electrons. The one-electron effective potential includes both the frozen-core Dirac-Hartree-Fock (DHF V^{N-2}) and self-energy (core-polarization) potentials. The self-energy correction is computed using second-order MBPT diagrams involving virtual core excitations. At the next step, the computed one-electron valence orbitals are used to diagonalize the atomic Hamiltonian in the model space of two valence electrons within the CI method. The CI model-space Hamiltonian includes the residual (beyond DHF) Coulomb interaction between the valence electrons and also their core-polarization-mediated interaction. The latter was computed in the second-order MBPT. This step yields two-electron wave-functions and energies. Finally, with the obtained wave-functions we calculated the required electric-dipole matrix elements. In calculations of transition rates we used experimental energy intervals and the computed CI+MBPT matrix elements.

We used two independent CI+MBPT implementations: (i) by the Reno group (see the description of the earlier version in Ref. [15]) and (ii) the recently published package [16]. The practical goal of the calculations was not reaching the best possible accuracy, but rather the generation of massive amounts of reliable data for the transition array involving 75 lowest-energy levels. The Reno code was run on a large basis set but without including core-polarization-mediated interaction in the CI Hamiltonian due to considerable computational costs. The production runs with package [16] employed a smaller basis set (due to code limitations) but treated the correlation problem more fully.

While using the package [16] we employed the one-electron basis set that included the $1s-17s$, $2p-17p$, $3d-17d$, $4f-17f$, and $5g-17g$ orbitals, where the core and $4s, \dots, 6f$ orbitals are DHF ones, while the remaining orbitals were represented by a B-spline basis set. The Reno code used the dual-kinetic-balance basis set generated in the DHF V^{N-2} potential using spherical cavity of 75 Bohr radius [17]. The basis included orbitals with orbital angular momentum ℓ up to 6. The total number of positive-energy (in the Dirac sense) orbitals per partial wave was 40 with the 35 lowest-energy orbitals used in the calculations.

For most states, the values of transition rates obtained with package [16] were in close agreement with the NIST recommended

values due to more complete treatment of the correlation problem. The level of agreement was degraded for states with the 4s6f electron configuration which was traced to our use of small basis set due to package [16] limitations. For these 4s6f states, the values of transition rates obtained with the Reno code displayed a better agreement with the NIST data because of the larger basis set. In addition, due to the restriction on the number of eigenvalues in the package [16], we were not able to compute the states arising from the 4s8s configuration. Our final values combine the outputs of the two codes. While the bulk of the results comes from the package [16], rates for states involving the 4s6f and 4s8s configurations are taken from the Reno code output in our tabulation. The rates for 4s7p ¹P₁ to 4s² ¹S₀, 4s7s ¹S₀ to 4s4p ¹P₁, and 4s6d ¹D₂ to 4s4p ¹P₁ transitions are taken from Reno code.

The spontaneous emission rate A_{if} from the upper (initial) state i to the lower (final) state f was calculated as

$$A_{if} = 2.02613 \times 10^{18} \frac{|\langle i||D||f\rangle|^2}{(2J_i + 1)\lambda^3} \text{ s}^{-1}, \quad (1)$$

where $\langle i||D||f\rangle$ is the reduced matrix element of the electric-dipole operator in atomic units, the transition wavelength λ is expressed in Å, and J_i is the total angular momentum of the upper (initial) state. The emission rate can be converted into the weighted oscillator strength using [18]

$$\begin{aligned} gf &= (2J_f + 1)f_{fi} = -(2J_i + 1)f_{if} \\ &= 1.499 \times 10^{-16} A_{if} \lambda^2 (2J_i + 1), \end{aligned} \quad (2)$$

where gf is weighted oscillator strength, f_{if} is the emission oscillator strength (usually taken to be negative), f_{fi} is the adsorption oscillator strength, and J_f is the total angular momentum of the lower (final) state. We determined λ from the NIST recommended energy values [19]. Finally, the total transition rate A_{total} from a given initial state is a sum of A_{if} over all E1-allowed final states, with the resulting initial state lifetime $\tau = 1/A_{\text{total}}$.

3. Results and discussion

We summarize the lifetime of the 75 states in Table 1 and compare with the available theoretical and experimental values. Our data show better agreement with the experimental values, as compared with the other theoretical data. The computed spontaneous emission rates are compiled in Tables 2–6. For completeness, we list values obtained with the electric dipole operator in both the length and velocity forms (gauges) in columns marked L and V , respectively. Generally, the length and velocity gauges agree at a few percent level, except for some occasional large discrepancies for weak transitions. The length form values are in better overall agreement with the available literature data and therefore we recommend using the length-form values.

We further assessed the quality of our calculation by comparing our values with other theoretical data [9–11] and with the NIST recommended values [19] in Table 7. The other theoretical data are taken primarily from three sources. The first source is the non-relativistic semi-empirical calculation by Hansen et al. [9]. They used the model potential and CI (MPCI) method to determine rates for the LS allowed E1 transitions for levels up to 4s10s. From a comparison with other semi-empirical work [6,7], Hansen et al. concluded that their data are more accurate because they have used larger basis size, larger cut-off radius, and more accurate model potential. In Table 7 we compare 80 transition rates with Hansen's results [9]. For comparison, their weighted oscillator strength gf values are converted to A_{if} (in 1/s) as $A_{if} = 6.67 \times 10^{15} gf / [(2J_i + 1)\lambda^2]$, where λ is in Å. The difference between our's and the Hansen's results is better than 1% for the 4s4p ¹P₁ – 4s² ¹S₀ and 4s4p ³P₁ – 4s² ¹S₀ transitions and better than 50%

for majority of other transitions. There are a few cases where the discrepancy between our's and Hansen's data is worse than 50% for some specific transitions decaying from highly excited states like 4sns with $n = 6-8$, 4s7p, 4s6d, and 4s5d. The second source is the *ab initio* relativistic MCHF calculations by Fischer et al. [10]. They report the transition rates between levels below 3d4p ¹F₃, both allowed and spin forbidden. In Table 7, we compared 13 spin forbidden singlet–triplet transition rates with their results. Our values are in better agreement with the NIST data than the MCHF results, for example, for the 4s4p ³P₁ – 4s² ¹S₀, 3d4p ¹D₂ – 3d4s ³D₁, 3d4p ¹D₂ – 3d4s ³D₂ transitions. The third source is the CI+MBPT calculation [11]. These authors reported rates for the spin-allowed 4s²–4s4p, 4s4p–3d4s transitions, and for the spin-forbidden 4s4p ¹P₁–4s5s ³S₁ and 4s4p ³P_{1,2}–3d4s ¹D₂ transitions. We find excellent agreement with their CI+MBPT results [11]. Finally, we compared 99 transition rates with the NIST Atomic Spectra Database [19] in Table 7. In most cases, the discrepancy is better than 50%. There are some instances when the discrepancy is worse than 50%. In particular, for the 4s6f ¹F₀ – 3d4s ¹D₂, 4s5p ¹P₁ – 4s² ¹S₀, and 4s4f ¹F₃ – 3d4s ¹D₂ transitions, our data show good agreement with the MPCI theoretical data, but display large differences with the NIST recommended values.

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Explanation of Tables

In Table 1, we compile radiative E1 lifetimes of the 74 lowest-energy excited states of Ca I. In Tables 2–6, we tabulate our theoretical data for spontaneous emission rates of all possible 811 E1-allowed transitions between the 75 lowest-energy states of Ca I. A comparison with other literature values is presented in Table 7.

Table 1. Radiative electric-dipole decay rates A_{total} and lifetimes τ of Ca I.

First column	States.
Second and third columns	Energies in cm^{-1} , our CI+MBPT and the NIST values.
Fourth column	Difference between our CI+MBPT and NIST energies in %.
Fifth column	Total spontaneous emission rates A_{total} in 10^8 s^{-1} for the state.
Sixth and seventh columns	Lifetime of the state, our and the literature values.
MPCI	Model Potential Configuration Interaction method.
MCHF	Multi-Configuration Hartree–Fock method.
Exp.	Experimental values.

Table 2. Spontaneous emission rates of transitions originating from the $4sns$ ($n = 4-8$) states of Ca I.

First and Second columns	Transition levels, the upper (initial) and the lower (final) level.
Third column	Transition wavelength λ , in nm.
Fourth and Fifth columns	Our values of spontaneous emission rates A_{ij} in 10^8 s^{-1} in length (L) and velocity (V) forms of the E1 operator.
Sixth column	Difference between the L and V column values defined as $(L - V)/L$ in %.
Seventh column	Branching ratio (BR) in %, defined as A_{ij}/A_{total} .

Table 3. Spontaneous emission rates of transitions originating from the $4snp$ ($n = 4-7$) states of Ca I.

First and Second columns	Transition levels, the upper (initial) and the lower (final) level.
Third column	Transition wavelength λ , in nm.
Fourth and Fifth columns	Our values of spontaneous emission rates A_{ij} in 10^8 s^{-1} in length (L) and velocity (V) forms of the E1 operator.
Sixth column	Difference between the L and V column values defined as $(L - V)/L$ in %.
Seventh column	Branching ratio (BR) in %, defined as A_{ij}/A_{total} .

Table 4. Spontaneous emission rates of transitions originating from the $4snd$ ($n = 3-6$) states of Ca I.

First and Second columns	Transition levels, the upper (initial) and the lower (final) level.
Third column	Transition wavelength λ , in nm.
Fourth and Fifth columns	Our values of spontaneous emission rates A_{ij} in 10^8 s^{-1} in length (L) and velocity (V) forms of the E1 operator.
Sixth column	Difference between the L and V column values defined as $(L - V)/L$ in %.
Seventh column	Branching ratio (BR) in %, defined as A_{ij}/A_{total} .

Table 5. Spontaneous emission rates of transitions originating from the $4snf$ ($n = 4-6$) states of Ca I.

First and Second columns	Transition levels, the upper (initial) and the lower (final) level.
Third column	Transition wavelength λ , in nm.
Fourth and Fifth columns	Our values of spontaneous emission rates A_{ij} in 10^8 s^{-1} in length (L) and velocity (V) forms of the E1 operator.
Sixth column	Difference between the L and V column values defined as $(L - V)/L$ in %.
Seventh column	Branching ratio (BR) in %, defined as A_{ij}/A_{total} .

Table 6. Spontaneous emission rates of transitions originating from the $3d^2$, $4p^2$, $3d4p$, and $4s5g$ states of Ca I.

First and Second columns	Transition levels, the upper (initial) and the lower (final) level.
Third column	Transition wavelength λ , in nm.
Fourth and Fifth columns	Our values of spontaneous emission rates A_{ij} in 10^8 s^{-1} in length (L) and velocity (V) forms of the E1 operator.
Sixth column	Difference between the L and V column values defined as $(L - V)/L$ in %.
Seventh column	Branching ratio (BR) in %, defined as A_{ij}/A_{total} .

Table 7. Comparison of transition probabilities with literature values.

First and Second columns	Transition levels, the upper (initial) and the lower (final) level.
Third column	Spontaneous emission rates A_{ij} in units of 10^8 s^{-1} using the L -form of the E1 operator.
Fourth and Fifth columns	Other theoretical A_{ij} values and the % difference between this work and other theoretical data, calculated as the difference of the third and fourth column values divided by the third column value.
Sixth and Seventh columns	NIST recommended A_{ij} value and the % difference between this work and NIST data, computed as the difference between the third and sixth column values divided by the third column value.
L	Length form of the electric-dipole operator.
MPCI	Model Potential Configuration Interaction method.
MCHF	Multi-Configuration Hartree–Fock method.
CI+MBPT	Configuration Interaction with Many-Body Perturbation Theory method.
NIST	NIST recommended values.

Table 1
Radiative electric-dipole decay rates A_{total} and lifetimes τ of Ca I.

State	Energy (cm ⁻¹)		Diff. (%)	$A_{\text{total}}(10^8 \text{ s}^{-1})$	τ (ns)		Refs.
	This work	NIST			This work		
4s4p ³ P ₀	15125.730	15157.900	0.2	0.0	∞		
4s4p ³ P ₁	15179.500	15210.060	0.2	2.74×10^{-5}	3.65×10^5	(3.4±0.2) × 10 ⁵ Exp. [20]	
4s4p ³ P ₂	15289.530	15315.940	0.2	0.0	∞		
3d4s ³ D ₁	20822.630	20335.360	2.4	8.68×10^{-3}	1.15×10^3		
3d4s ³ D ₂	20840.440	20349.260	2.4	8.50×10^{-3}	1.18×10^3		
3d4s ³ D ₃	20868.160	20371.000	2.4	8.24×10^{-3}	1.21×10^3		
3d4s ¹ D ₂	22449.920	21849.630	2.7	4.88×10^{-6}	2.05×10^6	2.3(5) × 10 ⁶ Exp. [21] 1.71(3) × 10 ⁶ Exp. [22] 4.535(28) Exp. [23]	
4s4p ¹ P ₁	23491.350	23652.300	0.7	2.17	4.61	12.4 MPCI [9]	
4s5s ³ S ₁	31729.740	31539.500	0.6	0.823	12.1		
4s5s ¹ S ₀	33465.560	33317.260	0.4	0.229	43.6		
3d4p ³ F ₂	36235.100	35730.450	1.4	0.401	24.9		
3d4p ³ F ₃	36332.400	35818.710	1.4	0.381	26.2		
3d4p ¹ D ₂	36350.570	35835.410	1.4	0.446	22.4		
3d4p ³ F ₄	36419.600	35896.890	1.5	0.385	26.0		
4s5p ³ P ₀	36513.680	36547.690	0.1	0.176	57.0		
4s5p ³ P ₁	36521.570	36554.750	0.1	0.176	56.9		
4s5p ³ P ₂	36543.800	36575.120	0.1	0.177	56.5		
4s5p ¹ P ₁	36708.430	36731.620	0.1	0.163	61.5	57.6 MPCI [9]	
4s4d ¹ D ₂	37660.590	37298.290	1.0	0.161	62.3	64.9 MPCI [9]	
4s4d ³ D ₁	38013.550	37748.200	0.7	0.786	12.7	13.0(5) Exp. [24]	
4s4d ³ D ₂	38017.720	37751.870	0.7	0.784	12.8	13.0(5) Exp. [24]	
4s4d ³ D ₃	38023.990	37757.450	0.7	0.781	12.8	13.0(5) Exp. [24]	
3d4p ³ D ₁	38787.640	38192.390	1.6	0.689	14.5		
3d4p ³ D ₂	38819.160	38219.120	1.6	0.690	14.5		
3d4p ³ D ₃	38866.410	38259.120	1.6	0.692	14.5		
4p ² ³ P ₀	38858.080	38417.540	1.1	1.83	5.48	6.9(4) Exp. [24]	
4p ² ³ P ₁	38908.680	38464.810	1.2	1.83	5.46	6.9(4) Exp. [24]	
4p ² ³ P ₂	39001.360	38551.560	1.2	1.83	5.45	6.9(4) Exp. [24]	
3d4p ³ P ₀	39871.870	39333.380	1.4	0.781	12.8		
3d4p ³ P ₁	39875.220	39335.320	1.4	0.781	12.8		
3d4p ³ P ₂	39883.770	39340.080	1.4	0.779	12.8		
4s6s ³ S ₁	40664.630	40474.240	0.5	0.327	30.6		
3d4p ¹ F ₃	41100.840	40537.890	1.4	0.073	137		
4s6s ¹ S ₀	40942.640	40690.440	0.6	0.070	142	113.0 MPCI [9]	
4p ² ¹ D ₂	41182.450	40719.850	1.1	0.593	16.9	15.2 MPCI [9] 16.3 Exp. [24]	
4s6p ¹ P ₁	41787.870	41679.010	0.3	0.361	27.7		
4p ² ¹ S ₀	42336.930	41786.280	1.3	0.792	12.6	12.5 MPCI [9] 14.4(7) Exp. [24]	
4s4f ³ F ₂	42078.450	42170.210	0.2	0.261	38.4		
4s4f ³ F ₃	42078.850	42170.560	0.2	0.261	38.4		
4s4f ³ F ₄	42079.380	42171.030	0.2	0.261	38.3		
4s4f ¹ F ₃	42392.680	42343.590	0.1	0.378	26.4	28.8 MPCI [9]	
4s6p ³ P ₀	42479.440	42514.850	0.1	0.005	0.020		
4s6p ³ P ₁	42483.640	42518.710	0.1	0.005	0.020		
4s6p ³ P ₂	42492.270	42526.590	0.1	0.005	0.019		
4s5d ³ D ₁	42979.530	42743.000	0.6	0.406	24.7		
4s5d ³ D ₂	42981.440	42744.720	0.6	0.405	24.7		
4s5d ³ D ₃	42984.390	42747.390	0.6	0.403	24.8		
4s5d ¹ D ₂	43227.380	42919.050	0.7	0.511	19.6	22.8 MPCI [9]	
3d ² ³ F ₂	44231.820	43474.830	1.7	0.007	0.015		
3d ² ³ F ₃	44251.410	43489.120	1.8	0.007	0.015		
3d ² ³ F ₄	44277.650	43508.090	1.8	0.007	0.015		
4snp ¹ P ₁	44382.940	43933.480	1.0	0.757	13.2		
4s7s ³ S ₁	44707.350	43980.770	1.7	0.223	44.9		
4s7s ¹ S ₀	45215.430	44276.540	2.1	0.248	40.4	73.2 MPCI [9] 45.7 MCHF [5]	
4s5f ³ F ₂	44796.860	44762.620	0.1	0.170	58.8		
4s5f ³ F ₃	44797.140	44762.840	0.1	0.170	58.8		
4s5f ³ F ₄	44797.520	44763.120	0.1	0.171	58.6		
4s5f ¹ F ₃	44870.500	44804.880	0.1	0.231	43.3	56.5 MPCI [9]	
4s5g ³ G ₅	45191.910	44874.860	0.7	0.005	195		
4s5g ¹ G ₄	45191.510	44875.950	0.7	0.007	147		
4s7p ³ P ₀	45997.520	44955.670	2.3	0.002	550		
4s7p ³ P ₁	46001.620	44957.660	2.3	0.002	546		
4s7p ³ P ₂	46010.100	44961.760	2.3	0.002	539		
4s6d ¹ D ₂	45815.480	44989.830	1.8	0.206	48.6	76.3 MPCI [9] 58.9 Exp. [25]	
4s6d ³ D ₁	45890.620	45049.070	1.9	0.378	26.5		

(continued on next page)

Table 1 (continued)

State	Energy (cm ⁻¹)		Diff. (%)	$A_{\text{total}}(10^8 \text{ s}^{-1})$	τ (ns)	
	This work	NIST			This work	Refs.
4s6d ³ D ₂	45893.340	45050.420	1.9	0.377	26.5	
4s6d ³ D ₃	45897.080	45052.370	1.9	0.376	26.6	
4s7p ¹ P ₁	46975.130	45425.360	3.4	0.407	24.5	
4s8s ³ S ₁		45738.680		0.009	105	149 MPCl [9] 118.3(6.3) Exp. [25]
4s8s ¹ S ₀		45887.200		0.006	157	
4s6f ³ F ₂	47711.820	46164.640	3.4	0.227	112.7	
4s6f ³ F ₃	47712.420	46164.790	3.4	0.228	113.7	
4s6f ³ F ₄	47713.200	46164.970	3.4	0.228	121.9	
4s6f ¹ F ₃	47768.330	46182.400	3.4	0.291	96.7	

Table 2
Spontaneous emission rates of transitions originating from the $4sns$ ($n = 4-8$) states of Ca I.

Transition		λ (nm)	$A_{if}(10^8 \text{ s}^{-1})$		Diff. (%)	BR. (%)
Initial	Final		L	V		
4s5s 3S_1	4s4p 3P_0	610.441	9.246E-02	9.001E-02	2.65	11.23
4s5s 3S_1	4s4p 3P_1	612.391	2.759E-01	2.685E-01	2.67	33.51
4s5s 3S_1	4s4p 3P_2	616.388	4.549E-01	4.426E-01	2.71	55.26
4s5s 3S_1	4s4p 1P_1	1267.877	5.911E-06	6.068E-06	-2.66	0.00
4s5s 1S_0	4s4p 3P_1	552.267	1.694E-05	1.826E-05	-7.78	0.01
4s5s 1S_0	4s4p 1P_1	1034.665	2.293E-01	2.217E-01	3.34	99.99
4s6s 3S_1	3d4p 3F_2	2108.019	2.378E-05	2.360E-05	0.77	0.01
4s6s 3S_1	3d4p 1D_2	2155.716	1.673E-04	1.664E-04	0.53	0.05
4s6s 3S_1	4s5p 3P_0	2546.765	9.152E-03	9.132E-03	0.22	2.80
4s6s 3S_1	4s5p 3P_1	2551.352	2.714E-02	2.708E-02	0.21	8.30
4s6s 3S_1	4s5p 3P_2	2564.681	4.537E-02	4.528E-02	0.21	13.88
4s6s 3S_1	4s5p 1P_1	2671.925	2.703E-04	2.697E-04	0.24	0.08
4s6s 3S_1	4s4p 3P_0	395.002	2.621E-02	2.500E-02	4.60	8.01
4s6s 3S_1	3d4p 3D_1	4382.409	5.498E-07	4.698E-07	14.55	0.00
4s6s 3S_1	3d4p 3D_2	4434.354	1.660E-06	1.531E-06	7.76	0.00
4s6s 3S_1	3d4p 3P_0	8765.317	1.184E-04	1.166E-04	1.53	0.04
4s6s 3S_1	4s4p 3P_1	395.817	7.994E-02	7.638E-02	4.46	24.45
4s6s 3S_1	3d4p 3P_1	8780.248	3.539E-04	3.462E-04	2.19	0.11
4s6s 3S_1	3d4p 3P_2	8817.098	5.849E-04	5.674E-04	2.99	0.18
4s6s 3S_1	4s4p 3P_2	397.483	1.377E-01	1.319E-01	4.20	42.10
4s6s 3S_1	4s4p 1P_1	594.462	1.172E-06	1.231E-06	-5.01	0.00
4s6s 1S_0	4s5p 3P_1	2417.976	5.790E-04	5.636E-04	2.67	0.82
4s6s 1S_0	4s5p 1P_1	2526.005	5.484E-02	5.299E-02	3.37	77.90
4s6s 1S_0	3d4p 3D_1	4003.122	8.321E-06	8.418E-06	-1.17	0.01
4s6s 1S_0	4s4p 3P_1	392.459	7.678E-04	8.401E-04	-9.42	1.09
4s6s 1S_0	3d4p 3P_1	7379.420	1.071E-06	8.795E-07	17.85	0.00
4s6s 1S_0	4s4p 1P_1	586.919	1.420E-02	2.181E-02	-53.58	20.17
4s7s 3S_1	3d4p 3F_2	1212.074	9.204E-06	9.121E-06	0.90	0.00
4s7s 3S_1	3d4p 1D_2	1227.693	6.343E-05	6.312E-05	0.48	0.03
4s7s 3S_1	4s5p 3P_0	1345.337	4.039E-03	4.043E-03	-0.12	1.81
4s7s 3S_1	4s5p 3P_1	1346.616	1.196E-02	1.197E-02	-0.13	5.37
4s7s 3S_1	4s5p 3P_2	1350.320	1.990E-02	1.994E-02	-0.16	8.94
4s7s 3S_1	4s5p 1P_1	1379.472	1.143E-04	1.145E-04	-0.22	0.05
4s7s 3S_1	4s4p 3P_0	346.947	1.873E-02	1.773E-02	5.35	8.41
4s7s 3S_1	3d4p 3D_1	1727.599	2.534E-08	1.214E-08	52.10	0.00
4s7s 3S_1	3d4p 3D_2	1735.614	6.215E-08	4.375E-08	29.61	0.00
4s7s 3S_1	3d4p 3P_0	2151.745	6.592E-05	5.724E-05	13.17	0.03
4s7s 3S_1	4s4p 3P_1	347.576	5.630E-02	5.330E-02	5.32	25.27
4s7s 3S_1	3d4p 3P_1	2152.644	2.023E-04	1.771E-04	12.49	0.09
4s7s 3S_1	3d4p 3P_2	2154.852	3.557E-04	3.143E-04	11.64	0.16
4s7s 3S_1	4s6p 1P_1	4344.502	3.555E-08	2.421E-08	31.91	0.00
4s7s 3S_1	4s4f 3F_2	5523.153	1.611E-13	1.419E-13	11.93	0.00
4s7s 3S_1	4s4p 3P_2	348.860	9.417E-02	8.923E-02	5.24	42.28
4s7s 3S_1	4s6p 3P_0	6821.655	1.886E-03	1.631E-03	13.50	0.85
4s7s 3S_1	4s6p 3P_1	6839.665	5.634E-03	4.869E-03	13.58	2.53
4s7s 3S_1	4s6p 3P_2	6876.728	9.311E-03	8.031E-03	13.75	4.18
4s7s 3S_1	4snp 1P_1	211461.197	6.064E-12	3.709E-10	-6016.54	0.00
4s7s 3S_1	4s4p 1P_1	491.921	7.761E-07	8.123E-07	-4.67	0.00
4s7s 1S_0	4s5p 3P_1	1295.037	4.787E-04	4.881E-04	-1.97	0.19
4s7s 1S_0	4s5p 1P_1	1325.395	4.599E-02	4.680E-02	-1.75	18.57
4s7s 1S_0	3d4p 3D_1	1643.615	1.933E-06	2.372E-06	-22.69	0.00
4s7s 1S_0	4s4p 3P_1	344.039	3.318E-06	3.419E-06	-3.03	0.00
4s7s 1S_0	3d4p 3P_1	2023.792	2.553E-08	4.952E-08	-93.96	0.00
4s7s 1S_0	4s6p 1P_1	3849.811	2.243E-02	1.991E-02	11.25	9.06
4s7s 1S_0	4s6p 3P_1	5688.832	3.489E-08	5.111E-08	-46.48	0.00
4s7s 1S_0	4snp 1P_1	29149.420	3.074E-04	9.826E-05	68.03	0.12
4s7s 1S_0	4s4p 1P_1	484.866	6.836E-02			72.05
4s8s 3S_1	3d4p 3F_2	999.178	7.736E-09			0.00
4s8s 3S_1	3d4p 1D_2	1009.767	7.664E-07			0.00
4s8s 3S_1	4s5p 3P_0	1088.022	1.542E-03			1.63
4s8s 3S_1	4s5p 3P_1	1088.858	4.577E-03			4.83
4s8s 3S_1	4s5p 3P_2	1091.279	7.690E-03			8.11
4s8s 3S_1	4s5p 1P_1	1110.240	4.267E-05			0.05
4s8s 3S_1	3d4p 3D_1	1325.154	5.676E-08			0.00
4s8s 3S_1	3d4p 3D_2	1329.865	2.426E-07			0.00
4s8s 3S_1	4s4p 3P_0	327.003	7.436E-03			7.85
4s8s 3S_1	3d4p 3P_0	1561.207	4.073E-05			0.04
4s8s 3S_1	3d4p 3P_1	1561.680	1.174E-04			0.12
4s8s 3S_1	3d4p 3P_2	1562.842	1.793E-04			0.19
4s8s 3S_1	4s4p 3P_1	327.561	2.225E-02			23.47

(continued on next page)

Table 2 (continued)

Transition		λ (nm)	$A_{if}(10^8 \text{ s}^{-1})$		Diff. (%)	BR. (%)
Initial	Final		L	V		
4s8s ³ S ₁	4s6p ¹ P ₁	2463.254	2.019E-08			0.00
4s8s ³ S ₁	4s4f ³ F ₂	2802.321	8.155E-13			0.00
4s8s ³ S ₁	4s4p ³ P ₂	328.701	3.693E-02			38.96
4s8s ³ S ₁	4s6p ³ P ₀	3101.901	8.286E-04			0.87
4s8s ³ S ₁	4s6p ³ P ₁	3105.619	2.469E-03			2.61
4s8s ³ S ₁	4s6p ³ P ₂	3113.238	4.063E-03			4.29
4s8s ³ S ₁	4snp ¹ P ₁	5539.552	1.078E-08			0.00
4s8s ³ S ₁	4s5f ³ F ₂	10245.272	2.432E-13			0.00
4s8s ³ S ₁	4s7p ³ P ₀	12771.229	7.410E-04			0.78
4s8s ³ S ₁	4s7p ³ P ₁	12803.769	2.215E-03			2.34
4s8s ³ S ₁	4s7p ³ P ₂	12871.338	3.664E-03			3.87
4s8s ³ S ₁	4s7p ¹ P ₁	31916.252	2.029E-08			0.00
4s8s ³ S ₁	4s4p ¹ P ₁	452.768	2.558E-07			0.00
4s8s ¹ S ₀	4s5p ³ P ₁	1071.530	1.821E-04			0.29
4s8s ¹ S ₀	4s5p ¹ P ₁	1092.230	1.964E-02			30.78
4s8s ¹ S ₀	3d4p ³ D ₁	1299.577	9.657E-06			0.02
4s8s ¹ S ₀	3d4p ³ P ₁	1526.279	7.658E-07			0.00
4s8s ¹ S ₀	4s4p ³ P ₁	325.976	6.115E-08			0.00
4s8s ¹ S ₀	4s6p ¹ P ₁	2376.319	6.149E-03			9.63
4s8s ¹ S ₀	4s6p ³ P ₁	2968.689	1.757E-07			0.00
4s8s ¹ S ₀	4snp ¹ P ₁	5118.441	7.344E-05			0.12
4s8s ¹ S ₀	4s7p ³ P ₁	10758.009	5.245E-07			0.00
4s8s ¹ S ₀	4s7p ¹ P ₁	21652.520	2.071E-03			3.25
4s8s ¹ S ₀	4s4p ¹ P ₁	449.743	3.569E-02			55.93

Table 3
Spontaneous emission rates of transitions originating from the $4snp$ ($n = 4-7$) states of Ca I.

Transition		λ (nm)	$A_{if}(10^8 \text{ s}^{-1})$		Diff. (%)	BR. (%)
Initial	Final		L	V		
4s4p 3P_1	4s 2 1S_0	657.460	2.738E-05	3.531E-05	-28.98	100.00
4s4p 1P_1	4s 2 1S_0	422.792	2.170E+00	2.327E+00	-7.20	100.00
4s4p 1P_1	3d4s 3D_1	3014.827	3.767E-08	4.832E-08	-28.27	0.00
4s4p 1P_1	3d4s 3D_2	3027.514	1.000E-07	3.825E-07	-282.52	0.00
4s4p 1P_1	3d4s 1D_2	5547.327	5.341E-05	2.287E-06	95.72	0.00
4s5p 3P_0	4s5s 3S_1	1996.729	7.103E-02	7.143E-02	-0.55	40.46
4s5p 3P_0	3d4s 3D_1	616.814	1.045E-01	1.102E-01	-5.38	59.54
4s5p 3P_1	4s5s 3S_1	1993.919	7.055E-02	7.096E-02	-0.58	40.15
4s5p 3P_1	4s 2 1S_0	273.562	2.340E-06	4.425E-05	-1790.81	0.00
4s5p 3P_1	4s5s 1S_0	3088.813	2.055E-04	2.050E-04	0.24	0.12
4s5p 3P_1	3d4s 3D_1	616.546	2.532E-02	2.667E-02	-5.34	14.41
4s5p 3P_1	3d4s 3D_2	617.075	7.859E-02	8.296E-02	-5.55	44.73
4s5p 3P_1	3d4s 1D_2	680.035	1.051E-03	1.177E-03	-11.99	0.60
4s5p 3P_2	4s5s 3S_1	1985.853	7.180E-02	7.223E-02	-0.60	40.59
4s5p 3P_2	3d4s 3D_1	615.773	6.273E-04	6.834E-04	-8.93	0.35
4s5p 3P_2	3d4s 3D_2	616.300	1.558E-02	1.638E-02	-5.14	8.81
4s5p 3P_2	3d4s 3D_3	617.127	8.710E-02	9.206E-02	-5.69	49.24
4s5p 3P_2	3d4s 1D_2	679.095	1.792E-03	2.000E-03	-11.62	1.01
4s5p 1P_1	4s5s 3S_1	1925.996	7.950E-04	7.974E-04	-0.30	0.49
4s5p 1P_1	4s 2 1S_0	272.245	7.505E-03	1.833E-02	-144.27	4.62
4s5p 1P_1	4s5s 1S_0	2928.807	2.361E-02	2.339E-02	0.95	14.52
4s5p 1P_1	3d4s 3D_1	609.895	3.978E-04	4.252E-04	-6.88	0.24
4s5p 1P_1	3d4s 3D_2	610.413	2.354E-04	2.298E-04	2.38	0.14
4s5p 1P_1	3d4s 1D_2	671.953	1.301E-01	1.446E-01	-11.19	79.98
4s6p 1P_1	4s5s 3S_1	986.241	5.599E-08	5.809E-08	-3.74	0.00
4s6p 1P_1	4s 2 1S_0	239.929	9.182E-02	8.164E-02	11.09	25.41
4s6p 1P_1	4s5s 1S_0	1195.922	1.516E-02	1.561E-02	-2.92	4.20
4s6p 1P_1	4s4d 1D_2	2282.730	1.407E-02	1.541E-02	-9.50	3.89
4s6p 1P_1	4s4d 3D_1	2544.005	2.339E-09	9.781E-09	-318.22	0.00
4s6p 1P_1	4s4d 3D_2	2546.382	1.725E-06	2.001E-06	-16.02	0.00
4s6p 1P_1	4p 2 3P_0	3066.102	2.017E-06	1.819E-06	9.82	0.00
4s6p 1P_1	4p 2 3P_1	3111.194	5.703E-09	4.304E-09	24.53	0.00
4s6p 1P_1	4p 2 3P_2	3197.493	7.016E-06	6.775E-06	3.43	0.00
4s6p 1P_1	4s6s 3S_1	8300.339	1.476E-08	1.402E-08	5.02	0.00
4s6p 1P_1	4s6s 1S_0	10115.622	1.605E-03	1.577E-03	1.75	0.44
4s6p 1P_1	4p 2 1D_2	10425.789	7.877E-04	6.658E-04	15.47	0.22
4s6p 1P_1	3d4s 3D_1	468.523	6.442E-07	1.470E-07	77.18	0.00
4s6p 1P_1	3d4s 3D_2	468.829	2.073E-05	2.677E-05	-29.15	0.01
4s6p 1P_1	3d4s 1D_2	504.302	2.379E-01	2.744E-01	-15.35	65.83
4s6p 3P_0	4s5s 3S_1	911.133	7.945E-03	8.043E-03	-1.23	15.61
4s6p 3P_0	4s4d 3D_1	2097.909	7.984E-03	7.472E-03	6.42	15.69
4s6p 3P_0	4p 2 3P_1	2469.111	4.647E-06	1.928E-06	58.52	0.01
4s6p 3P_0	4s6s 3S_1	4900.495	1.618E-02	1.650E-02	-1.97	31.79
4s6p 3P_0	3d4s 3D_1	450.867	1.878E-02	2.995E-02	-59.42	36.90
4s6p 3P_1	4s5s 3S_1	910.812	8.107E-03	8.203E-03	-1.19	15.85
4s6p 3P_1	4s 2 1S_0	235.191	1.122E-08	4.799E-08	-327.69	0.00
4s6p 3P_1	4s5s 1S_0	1086.785	1.281E-08	3.164E-08	-146.98	0.00
4s6p 3P_1	4s4d 1D_2	1915.555	2.977E-07	2.213E-07	25.66	0.00
4s6p 3P_1	4s4d 3D_1	2096.212	1.976E-03	1.848E-03	6.49	3.86
4s6p 3P_1	4s4d 3D_2	2097.826	5.964E-03	5.579E-03	6.45	11.66
4s6p 3P_1	4p 2 3P_0	2438.329	2.340E-08	6.862E-08	-193.25	0.00
4s6p 3P_1	4p 2 3P_1	2466.760	6.170E-07	1.982E-07	67.88	0.00
4s6p 3P_1	4p 2 3P_2	2520.701	1.270E-06	3.888E-07	69.38	0.00
4s6p 3P_1	4s6s 3S_1	4891.243	1.625E-02	1.657E-02	-1.96	31.78
4s6p 3P_1	4s6s 1S_0	5469.652	2.777E-08	3.211E-08	-15.61	0.00
4s6p 3P_1	4p 2 1D_2	5559.076	9.162E-09	5.895E-09	35.66	0.00
4s6p 3P_1	4p 2 1S_0	13653.182	5.670E-10	3.303E-10	41.75	0.00
4s6p 3P_1	3d4s 3D_1	450.789	4.808E-03	7.627E-03	-58.62	9.40
4s6p 3P_1	3d4s 3D_2	451.071	1.403E-02	2.241E-02	-59.70	27.43
4s6p 3P_1	3d4s 1D_2	483.814	2.442E-06	2.156E-06	11.73	0.00
4s6p 3P_2	4s5s 3S_1	910.159	8.442E-03	8.542E-03	-1.18	16.34
4s6p 3P_2	4s4d 1D_2	1912.668	1.141E-07	1.298E-07	-13.73	0.00
4s6p 3P_2	4s4d 3D_1	2092.755	7.728E-05	7.217E-05	6.62	0.15
4s6p 3P_2	4s4d 3D_2	2094.364	1.168E-03	1.091E-03	6.57	2.26
4s6p 3P_2	4s4d 3D_3	2096.814	6.602E-03	6.170E-03	6.54	12.78
4s6p 3P_2	4p 2 3P_1	2461.975	9.452E-07	1.747E-06	-84.89	0.00
4s6p 3P_2	4p 2 3P_2	2515.704	1.001E-08	4.894E-07	-4791.12	0.00
4s6p 3P_2	4s6s 3S_1	4872.463	1.638E-02	1.671E-02	-1.99	31.71
4s6p 3P_2	4p 2 1D_2	5534.831	1.361E-08	1.069E-08	21.42	0.00
4s6p 3P_2	3d4s 3D_1	450.628	2.012E-04	3.163E-04	-57.22	0.39

(continued on next page)

Table 3 (continued)

Transition		λ (nm)	$A_{if}(10^8 \text{ s}^{-1})$		Diff. (%)	BR. (%)
Initial	Final		L	V		
4s6p ³ P ₂	3d4s ³ D ₂	450.911	2.942E-03	4.653E-03	-58.15	5.69
4s6p ³ P ₂	3d4s ³ D ₃	451.353	1.585E-02	2.530E-02	-59.67	30.67
4s6p ³ P ₂	3d4s ¹ D ₂	483.630	3.466E-06	4.781E-06	-37.96	0.01
4snp ¹ P ₁	4s5s ³ S ₁	806.843	1.985E-07	1.391E-07	29.94	0.00
4snp ¹ P ₁	4s ² ¹ S ₀	227.617	3.246E-01	3.466E-01	-6.80	42.88
4snp ¹ P ₁	4s5s ¹ S ₀	941.955	3.895E-02	4.001E-02	-2.71	5.15
4snp ¹ P ₁	4s4d ¹ D ₂	1507.116	1.273E-02	1.509E-02	-18.48	1.68
4snp ¹ P ₁	4s4d ³ D ₁	1616.742	6.691E-09	2.113E-08	-215.79	0.00
4snp ¹ P ₁	4s4d ³ D ₂	1617.702	1.500E-06	1.628E-06	-8.50	0.00
4snp ¹ P ₁	4p ² ³ P ₀	1812.928	5.659E-08	2.200E-08	61.12	0.00
4snp ¹ P ₁	4p ² ³ P ₁	1828.598	6.298E-09	1.871E-08	-197.07	0.00
4snp ¹ P ₁	4p ² ³ P ₂	1858.073	1.206E-06	1.524E-06	-26.37	0.00
4snp ¹ P ₁	4s6s ³ S ₁	2890.808	8.702E-08	1.053E-07	-21.02	0.00
4snp ¹ P ₁	4s6s ¹ S ₀	3083.527	6.961E-03	7.698E-03	-10.59	0.92
4snp ¹ P ₁	4p ² ¹ D ₂	3111.746	7.630E-04	8.518E-04	-11.63	0.10
4snp ¹ P ₁	4p ² ¹ S ₀	4657.228	3.175E-03	3.202E-03	-0.85	0.42
4snp ¹ P ₁	4s5d ³ D ₁	8399.973	1.344E-08	1.665E-08	-23.86	0.00
4snp ¹ P ₁	4s5d ³ D ₂	8412.127	2.373E-07	1.846E-07	22.23	0.00
4snp ¹ P ₁	4s5d ¹ D ₂	9857.753	2.552E-03	2.015E-03	21.02	0.34
4snp ¹ P ₁	3d ² ³ F ₂	21803.118	2.171E-08	1.501E-08	30.87	0.00
4snp ¹ P ₁	3d4s ³ D ₁	423.763	7.516E-07	2.790E-07	62.87	0.00
4snp ¹ P ₁	3d4s ³ D ₂	424.012	5.665E-06	5.933E-06	-4.74	0.00
4snp ¹ P ₁	3d4s ¹ D ₂	452.820	3.673E-01	4.427E-01	-20.53	48.52
4s7p ³ P ₀	4s5s ³ S ₁	745.369	1.781E-03	1.925E-03	-8.08	9.79
4s7p ³ P ₀	4s4d ³ D ₁	1387.449	5.557E-03	5.436E-03	2.17	30.55
4s7p ³ P ₀	4p ² ³ P ₁	1540.628	3.888E-06	3.340E-06	14.10	0.02
4s7p ³ P ₀	4s6s ³ S ₁	2231.431	2.027E-03	1.651E-03	18.56	11.14
4s7p ³ P ₀	4s5d ³ D ₁	4519.427	4.666E-03	2.823E-03	39.50	25.66
4s7p ³ P ₀	3d4s ³ D ₁	406.169	1.349E-03	3.243E-03	-140.39	7.42
4s7p ³ P ₀	4s7s ³ S ₁	10257.462	2.804E-03	4.161E-03	-48.38	15.42
4s7p ³ P ₁	4s5s ³ S ₁	745.259	1.866E-03	2.014E-03	-7.91	10.19
4s7p ³ P ₁	4s ² ¹ S ₀	222.432	2.344E-07	3.119E-08	86.69	0.00
4s7p ³ P ₁	4s5s ¹ S ₀	859.077	7.106E-08	3.350E-08	52.85	0.00
4s7p ³ P ₁	4s4d ¹ D ₂	1305.590	4.279E-07	3.715E-07	13.17	0.00
4s7p ³ P ₁	4s4d ³ D ₁	1387.066	1.376E-03	1.346E-03	2.22	7.52
4s7p ³ P ₁	4s4d ³ D ₂	1387.773	4.153E-03	4.062E-03	2.19	22.68
4s7p ³ P ₁	4p ² ³ P ₀	1529.024	5.358E-08	2.853E-08	46.76	0.00
4s7p ³ P ₁	4p ² ³ P ₁	1540.156	5.720E-07	4.865E-07	14.96	0.00
4s7p ³ P ₁	4p ² ³ P ₂	1561.012	1.080E-06	8.977E-07	16.87	0.01
4s7p ³ P ₁	4s6s ³ S ₁	2230.440	2.065E-03	1.684E-03	18.47	11.28
4s7p ³ P ₁	4s6s ¹ S ₀	2343.446	5.201E-09	7.345E-09	-41.23	0.00
4s7p ³ P ₁	4p ² ¹ D ₂	2359.709	6.693E-09	1.793E-08	-167.98	0.00
4s7p ³ P ₁	4p ² ¹ S ₀	3153.201	1.366E-07	1.495E-07	-9.47	0.00
4s7p ³ P ₁	4s5d ³ D ₁	4515.366	1.159E-03	7.005E-04	39.58	6.33
4s7p ³ P ₁	4s5d ³ D ₂	4518.875	3.489E-03	2.109E-03	39.57	19.05
4s7p ³ P ₁	4s5d ¹ D ₂	4905.303	9.373E-08	7.250E-08	22.64	0.00
4s7p ³ P ₁	3d ² ³ F ₂	6743.861	1.526E-11	2.413E-13	98.42	0.00
4s7p ³ P ₁	3d4s ³ D ₁	406.136	3.506E-04	8.310E-04	-137.01	1.91
4s7p ³ P ₁	4s7s ³ S ₁	10236.567	2.815E-03	4.179E-03	-48.48	15.37
4s7p ³ P ₁	4s7s ¹ S ₀	14681.701	6.269E-08	8.214E-08	-31.03	0.00
4s7p ³ P ₁	3d4s ³ D ₂	406.365	1.029E-03	2.465E-03	-139.62	5.62
4s7p ³ P ₁	3d4s ¹ D ₂	432.750	4.981E-06	5.234E-06	-5.06	0.03
4s7p ³ P ₂	4s5s ³ S ₁	745.031	2.047E-03	2.203E-03	-7.63	11.03
4s7p ³ P ₂	4s4d ¹ D ₂	1304.892	8.304E-08	9.558E-08	-15.10	0.00
4s7p ³ P ₂	4s4d ³ D ₁	1386.278	5.391E-05	5.267E-05	2.30	0.29
4s7p ³ P ₂	4s4d ³ D ₂	1386.984	8.143E-04	7.958E-04	2.27	4.39
4s7p ³ P ₂	4s4d ³ D ₃	1388.058	4.603E-03	4.500E-03	2.24	24.81
4s7p ³ P ₂	4p ² ³ P ₁	1539.184	4.980E-07	5.495E-07	-10.35	0.00
4s7p ³ P ₂	4p ² ³ P ₂	1560.014	1.123E-08	4.110E-10	96.34	0.00
4s7p ³ P ₂	4s6s ³ S ₁	2228.402	2.145E-03	1.752E-03	18.29	11.56
4s7p ³ P ₂	4p ² ¹ D ₂	2357.429	6.802E-09	7.577E-09	-11.39	0.00
4s7p ³ P ₂	4s5d ³ D ₁	4507.022	4.580E-05	2.759E-05	39.75	0.25
4s7p ³ P ₂	4s5d ³ D ₂	4510.519	6.890E-04	4.152E-04	39.74	3.71
4s7p ³ P ₂	4s5d ³ D ₃	4515.957	3.876E-03	2.337E-03	39.71	20.89
4s7p ³ P ₂	4s5d ¹ D ₂	4895.458	1.470E-07	8.716E-08	40.69	0.00
4s7p ³ P ₂	3d ² ³ F ₂	6725.266	1.161E-13	2.007E-12	-1627.75	0.00
4s7p ³ P ₂	3d4s ³ D ₁	406.068	1.509E-05	3.487E-05	-131.15	0.08
4s7p ³ P ₂	3d ² ³ F ₃	6790.526	3.141E-15	1.968E-11		0.00
4s7p ³ P ₂	4s7s ³ S ₁	10193.784	2.836E-03	4.219E-03	-48.74	15.29
4s7p ³ P ₂	3d4s ³ D ₂	406.298	2.219E-04	5.176E-04	-133.28	1.20
4s7p ³ P ₂	3d4s ³ D ₃	406.657	1.204E-03	2.852E-03	-136.81	6.49

(continued on next page)

Table 3 (continued)

Transition		λ (nm)	$A_{if}(10^8 \text{ s}^{-1})$		Diff. (%)	BR. (%)
Initial	Final		L	V		
4s7p ³ P ₂	3d4s ¹ D ₂	432.673	7.948E-08	2.350E-07	-195.65	0.00
4s7p ¹ P ₁	4s5s ³ S ₁	720.157	1.497E-06	1.062E-06	29.07	0.00
4s7p ¹ P ₁	4s ² ¹ S ₀	220.141	1.295E-01			55.13
4s7p ¹ P ₁	4s5s ¹ S ₀	825.893	1.135E-02	1.209E-02	-6.49	2.79
4s7p ¹ P ₁	4s4d ¹ D ₂	1230.456	4.083E-03	5.034E-03	-23.28	1.00
4s7p ¹ P ₁	4s4d ³ D ₁	1302.565	1.678E-09	1.352E-08	-705.49	0.00
4s7p ¹ P ₁	4s4d ³ D ₂	1303.188	2.058E-07	2.067E-07	-0.45	0.00
4s7p ¹ P ₁	4p ² ³ P ₀	1426.977	5.766E-07	4.382E-07	24.01	0.00
4s7p ¹ P ₁	4p ² ³ P ₁	1436.668	3.708E-08	1.279E-07	-245.02	0.00
4s7p ¹ P ₁	4p ² ³ P ₂	1454.799	2.469E-07	1.081E-06	-337.68	0.00
4s7p ¹ P ₁	4s6s ³ S ₁	2019.745	7.975E-07	6.883E-07	13.69	0.00
4s7p ¹ P ₁	4s6s ¹ S ₀	2111.968	4.763E-03	4.261E-03	10.53	1.17
4s7p ¹ P ₁	4p ² ¹ D ₂	2125.168	1.349E-03	1.870E-03	-38.60	0.33
4s7p ¹ P ₁	4p ² ¹ S ₀	2747.947	7.203E-07	5.423E-05	-7429.71	0.00
4s7p ¹ P ₁	4s5d ³ D ₁	3728.060	5.631E-09	4.271E-10	92.42	0.00
4s7p ¹ P ₁	4s5d ³ D ₂	3730.452	1.906E-10	3.758E-09	-1872.01	0.00
4s7p ¹ P ₁	4s5d ¹ D ₂	3989.929	7.689E-04	1.177E-04	84.70	0.19
4s7p ¹ P ₁	3d ² ³ F ₂	5126.812	3.402E-07	1.639E-07	51.81	0.00
4s7p ¹ P ₁	3d4s ³ D ₁	398.565	1.918E-09	3.078E-08	-1504.30	0.00
4s7p ¹ P ₁	4s7s ³ S ₁	6922.379	2.786E-07	5.027E-07	-80.46	0.00
4s7p ¹ P ₁	4s7s ¹ S ₀	8704.584	2.597E-03	4.065E-03	-56.57	0.64
4s7p ¹ P ₁	3d4s ³ D ₂	398.786	1.169E-05	1.428E-05	-22.12	0.00
4s7p ¹ P ₁	4s6d ¹ D ₂	22960.531	4.250E-04	1.325E-04	68.83	0.10
4s7p ¹ P ₁	4s6d ³ D ₁	26575.248	6.286E-09	3.545E-09	43.61	0.00
4s7p ¹ P ₁	4s6d ³ D ₂	26670.934	6.608E-07	1.930E-07	70.80	0.00
4s7p ¹ P ₁	3d4s ¹ D ₂	424.165	1.575E-01	1.942E-01	-23.35	38.64

Table 4
Spontaneous emission rates of transitions originating from the 4snd ($n = 3-6$) states of Ca I.

Transition		λ (nm)	A_{if} (10^8 s^{-1})		Diff. (%)	BR. (%)
Initial	Final		L	V		
3d4s 3D_1	4s4p 3P_0	1931.449	4.891E-03	4.940E-03	-0.99	56.36
3d4s 3D_1	4s4p 3P_1	1951.105	3.564E-03	3.604E-03	-1.11	41.06
3d4s 3D_1	4s4p 3P_2	1992.262	2.239E-04	2.271E-04	-1.46	2.58
3d4s 3D_2	4s4p 3P_1	1945.828	6.467E-03	6.537E-03	-1.07	76.09
3d4s 3D_2	4s4p 3P_2	1986.760	2.032E-03	2.060E-03	-1.37	23.91
3d4s 3D_3	4s4p 3P_2	1978.216	8.240E-03	8.340E-03	-1.22	100.00
3d4s 1D_2	4s4p 3P_1	1506.122	4.059E-06	3.854E-06	5.05	83.12
3d4s 1D_2	4s4p 3P_2	1530.529	8.245E-07	4.298E-07	47.87	16.88
4s4d 1D_2	3d4p 3F_2	6378.202	1.341E-05	4.334E-06	67.69	0.01
4s4d 1D_2	3d4p 3F_3	6758.675	2.997E-12	9.405E-10		0.00
4s4d 1D_2	3d4p 1D_2	6835.831	2.778E-05	7.399E-06	73.37	0.02
4s4d 1D_2	4s5p 3P_1	13449.176	3.410E-06	3.878E-06	-13.75	0.00
4s4d 1D_2	4s5p 3P_2	13828.007	3.794E-08	1.751E-08	53.85	0.00
4s4d 1D_2	4s5p 1P_1	17646.955	1.270E-04	1.479E-04	-16.46	0.08
4s4d 1D_2	4s4p 3P_1	452.730	4.043E-06	2.354E-06	41.76	0.00
4s4d 1D_2	4s4p 3P_2	454.910	2.657E-04	2.853E-04	-7.37	0.17
4s4d 1D_2	4s4p 1P_1	732.816	1.601E-01	1.521E-01	5.04	99.73
4s4d 3D_1	3d4p 3F_2	4956.015	8.657E-05	3.087E-04	-256.62	0.01
4s4d 3D_1	3d4p 1D_2	5227.965	2.133E-05	9.554E-05	-347.94	0.00
4s4d 3D_1	4s5p 3P_0	8329.793	8.753E-04	8.950E-04	-2.25	0.11
4s4d 3D_1	4s5p 3P_1	8379.069	6.389E-04	6.531E-04	-2.23	0.08
4s4d 3D_1	4s5p 3P_2	8524.568	4.144E-05	4.311E-05	-4.02	0.01
4s4d 3D_1	4s5p 1P_1	9836.904	4.067E-06	4.195E-06	-3.15	0.00
4s4d 3D_1	4s4p 3P_0	442.668	4.415E-01	4.444E-01	-0.66	56.18
4s4d 3D_1	4s4p 3P_1	443.692	3.223E-01	3.239E-01	-0.50	41.01
4s4d 3D_1	4s4p 3P_2	445.787	2.034E-02	2.038E-02	-0.19	2.59
4s4d 3D_1	4s4p 1P_1	709.426	1.472E-05	1.545E-05	-4.93	0.00
4s4d 3D_2	3d4p 3F_2	4947.017	4.947E-06	2.471E-05	-399.44	0.00
4s4d 3D_2	3d4p 3F_3	5172.878	9.036E-05	3.505E-04	-287.87	0.01
4s4d 3D_2	3d4p 1D_2	5217.954	1.436E-05	3.049E-05	-112.32	0.00
4s4d 3D_2	4s5p 3P_1	8353.381	1.159E-03	1.185E-03	-2.32	0.15
4s4d 3D_2	4s5p 3P_2	8497.982	3.700E-04	3.778E-04	-2.11	0.05
4s4d 3D_2	4s5p 1P_1	9801.519	8.902E-06	9.008E-06	-1.20	0.00
4s4d 3D_2	4s4p 3P_1	443.620	5.939E-01	5.979E-01	-0.66	75.78
4s4d 3D_2	4s4p 3P_2	445.714	1.882E-01	1.889E-01	-0.38	24.01
4s4d 3D_2	4s4p 1P_1	709.241	5.037E-05	4.876E-05	3.20	0.01
4s4d 3D_3	3d4p 3F_2	4933.399	4.148E-06	6.231E-06	-50.22	0.00
4s4d 3D_3	3d4p 3F_3	5157.989	8.396E-06	3.183E-05	-279.06	0.00
4s4d 3D_3	3d4p 1D_2	5202.805	1.347E-05	1.265E-05	6.12	0.00
4s4d 3D_3	3d4p 3F_4	5374.726	8.476E-05	3.470E-04	-309.41	0.01
4s4d 3D_3	4s5p 3P_2	8457.876	1.506E-03	1.542E-03	-2.44	0.19
4s4d 3D_3	4s4p 3P_2	445.603	7.793E-01	7.841E-01	-0.62	99.79
4s5d 3D_1	3d4p 3F_2	1426.015	5.674E-04	9.580E-04	-68.85	0.14
4s5d 3D_1	3d4p 1D_2	1447.683	2.901E-04	4.608E-04	-58.87	0.07
4s5d 3D_1	4s5p 3P_0	1614.124	2.721E-02	2.712E-02	0.35	6.71
4s5d 3D_1	4s5p 3P_1	1615.966	2.024E-02	2.017E-02	0.34	4.99
4s5d 3D_1	4s5p 3P_2	1621.303	1.351E-03	1.341E-03	0.71	0.33
4s5d 3D_1	4s5p 1P_1	1663.512	2.278E-04	2.272E-04	0.29	0.06
4s5d 3D_1	4s4p 3P_0	362.515	1.927E-01	1.949E-01	-1.17	47.50
4s5d 3D_1	3d4p 3D_1	2197.508	3.832E-04	3.482E-04	9.15	0.09
4s5d 3D_1	3d4p 3D_2	2210.492	1.230E-04	1.118E-04	9.10	0.03
4s5d 3D_1	3d4p 3P_0	2932.878	3.953E-03	4.409E-03	-11.52	0.97
4s5d 3D_1	4s4p 3P_1	363.201	1.452E-01	1.469E-01	-1.17	35.80
4s5d 3D_1	3d4p 3P_1	2934.548	2.947E-03	3.285E-03	-11.49	0.73
4s5d 3D_1	3d4p 3P_2	2938.653	1.943E-04	2.166E-04	-11.48	0.05
4s5d 3D_1	4s6p 1P_1	9398.585	7.140E-09	1.133E-08	-58.67	0.00
4s5d 3D_1	4s4f 3F_2	17458.405	4.014E-04	3.943E-04	1.77	0.10
4s5d 3D_1	4s4p 3P_2	364.603	9.773E-03	9.890E-03	-1.20	2.41
4s5d 3D_1	4s6p 3P_0	43830.813	2.419E-05	3.547E-05	-46.67	0.01
4s5d 3D_1	4s6p 3P_1	44585.135	1.724E-05	2.545E-05	-47.63	0.00
4s5d 3D_1	4s6p 3P_2	46208.586	1.033E-06	1.547E-06	-49.79	0.00
4s5d 3D_1	4s4p 1P_1	523.815	4.670E-06	5.065E-06	-8.45	0.00
4s5d 3D_2	3d4p 3F_2	1425.665	1.123E-04	1.667E-04	-48.50	0.03
4s5d 3D_2	3d4p 3F_3	1443.833	7.112E-04	1.197E-03	-68.34	0.18
4s5d 3D_2	3d4p 1D_2	1447.323	1.035E-06	3.266E-07	68.44	0.00
4s5d 3D_2	4s5p 3P_1	1615.517	3.645E-02	3.632E-02	0.36	9.01
4s5d 3D_2	4s5p 3P_2	1620.851	1.231E-02	1.227E-02	0.27	3.04
4s5d 3D_2	4s5p 1P_1	1663.036	2.945E-04	2.945E-04	0.02	0.07
4s5d 3D_2	3d4p 3D_1	2196.677	4.749E-05	4.072E-05	14.27	0.01
4s5d 3D_2	3d4p 3D_2	2209.652	3.503E-04	3.173E-04	9.44	0.09

(continued on next page)

Table 4 (continued)

Transition		λ (nm)	A_{if} (10^8 s^{-1})		Diff. (%)	BR. (%)
Initial	Final		L	V		
4s5d ³ D ₂	3d4p ³ D ₃	2229.356	7.036E-05	6.352E-05	9.73	0.02
4s5d ³ D ₂	4s4p ³ P ₁	363.179	2.593E-01	2.624E-01	-1.18	64.09
4s5d ³ D ₂	3d4p ³ P ₁	2933.067	5.367E-03	5.986E-03	-11.54	1.33
4s5d ³ D ₂	3d4p ³ P ₂	2937.168	1.768E-03	1.971E-03	-11.51	0.44
4s5d ³ D ₂	3d4p ¹ F ₃	4531.387	1.324E-07	1.016E-07	23.28	0.00
4s5d ³ D ₂	4s6p ¹ P ₁	9383.416	3.239E-07	3.478E-07	-7.38	0.00
4s5d ³ D ₂	4s4f ³ F ₂	17406.137	4.516E-05	4.435E-05	1.79	0.01
4s5d ³ D ₂	4s4f ³ F ₃	17416.748	3.588E-04	3.525E-04	1.76	0.09
4s5d ³ D ₂	4s4p ³ P ₂	364.581	8.734E-02	8.839E-02	-1.20	21.59
4s5d ³ D ₂	4s4f ¹ F ₃	24929.574	1.528E-08	1.641E-08	-7.36	0.00
4s5d ³ D ₂	4s6p ³ P ₁	44245.830	3.176E-05	4.678E-05	-47.29	0.01
4s5d ³ D ₂	4s6p ³ P ₂	45844.221	9.520E-06	1.422E-05	-49.42	0.00
4s5d ³ D ₂	4s4p ¹ P ₁	523.768	2.267E-05	2.414E-05	-6.45	0.01
4s5d ³ D ₃	3d4p ³ F ₂	1425.123	1.057E-05	8.168E-06	22.72	0.00
4s5d ³ D ₃	3d4p ³ F ₃	1443.276	6.712E-05	1.117E-04	-66.44	0.02
4s5d ³ D ₃	3d4p ¹ D ₂	1446.763	1.651E-04	1.682E-04	-1.83	0.04
4s5d ³ D ₃	3d4p ³ F ₄	1459.747	7.044E-04	1.199E-03	-70.24	0.17
4s5d ³ D ₃	4s5p ³ P ₂	1620.149	4.895E-02	4.878E-02	0.36	12.15
4s5d ³ D ₃	3d4p ³ D ₂	2208.349	2.401E-05	1.934E-05	19.47	0.01
4s5d ³ D ₃	3d4p ³ D ₃	2228.030	3.871E-04	3.443E-04	11.04	0.10
4s5d ³ D ₃	3d4p ³ P ₂	2934.867	7.191E-03	8.024E-03	-11.59	1.78
4s5d ³ D ₃	3d4p ¹ F ₃	4525.911	1.350E-08	1.565E-08	-15.96	0.00
4s5d ³ D ₃	4s4f ³ F ₂	17325.618	9.287E-07	9.121E-07	1.79	0.00
4s5d ³ D ₃	4s4f ³ F ₃	17336.130	3.247E-05	3.190E-05	1.77	0.01
4s5d ³ D ₃	4s4p ³ P ₂	364.545	3.451E-01	3.494E-01	-1.23	85.62
4s5d ³ D ₃	4s4f ³ F ₄	17350.267	3.751E-04	3.686E-04	1.74	0.09
4s5d ³ D ₃	4s4f ¹ F ₃	24764.735	1.063E-11	4.116E-14	99.61	0.00
4s5d ³ D ₃	4s6p ³ P ₂	45289.855	3.953E-05	5.883E-05	-48.82	0.01
4s5d ¹ D ₂	3d4p ³ F ₂	1391.091	3.178E-04	5.393E-04	-69.70	0.06
4s5d ¹ D ₂	3d4p ³ F ₃	1408.383	1.842E-07	9.196E-08	50.07	0.00
4s5d ¹ D ₂	3d4p ¹ D ₂	1411.704	6.727E-04	1.171E-03	-74.00	0.13
4s5d ¹ D ₂	4s5p ³ P ₁	1571.265	2.494E-04	2.510E-04	-0.64	0.05
4s5d ¹ D ₂	4s5p ³ P ₂	1576.310	1.835E-07	7.977E-07	-334.59	0.00
4s5d ¹ D ₂	4s5p ¹ P ₁	1616.180	3.302E-02	3.328E-02	-0.79	6.46
4s5d ¹ D ₂	3d4p ³ D ₁	2115.659	6.374E-06	6.799E-06	-6.66	0.00
4s5d ¹ D ₂	3d4p ³ D ₂	2127.691	2.942E-07	2.245E-07	23.69	0.00
4s5d ¹ D ₂	3d4p ³ D ₃	2145.955	1.764E-08	5.117E-08	-190.06	0.00
4s5d ¹ D ₂	4s4p ³ P ₁	360.894	4.989E-06	5.512E-06	-10.48	0.00
4s5d ¹ D ₂	3d4p ³ P ₁	2790.389	2.158E-06	2.145E-06	0.61	0.00
4s5d ¹ D ₂	3d4p ³ P ₂	2794.100	5.239E-07	7.264E-07	-38.65	0.00
4s5d ¹ D ₂	3d4p ¹ F ₃	4199.634	1.274E-03	9.537E-04	25.14	0.25
4s5d ¹ D ₂	4s6p ¹ P ₁	8064.256	4.324E-03	4.715E-03	-9.06	0.85
4s5d ¹ D ₂	4s4f ³ F ₂	13353.988	1.317E-08	1.371E-08	-4.12	0.00
4s5d ¹ D ₂	4s4f ³ F ₃	13360.232	7.626E-08	7.525E-08	1.33	0.00
4s5d ¹ D ₂	4s4p ³ P ₂	362.278	9.190E-06	1.055E-05	-14.76	0.00
4s5d ¹ D ₂	4s4f ¹ F ₃	17377.402	3.433E-04	3.685E-04	-7.32	0.07
4s5d ¹ D ₂	4s6p ³ P ₁	24978.768	2.028E-08	2.336E-08	-15.19	0.00
4s5d ¹ D ₂	4s6p ³ P ₂	25480.304	8.673E-09	9.809E-09	-13.10	0.00
4s5d ¹ D ₂	4s4p ¹ P ₁	519.029	4.710E-01	4.953E-01	-5.16	92.13
4s6d ¹ D ₂	3d4p ³ F ₂	1079.986	6.757E-06	8.174E-05	-1109.68	0.00
4s6d ¹ D ₂	3d4p ³ F ₃	1090.379	1.109E-05	1.180E-05	-6.38	0.01
4s6d ¹ D ₂	3d4p ¹ D ₂	1092.368	5.667E-05	3.284E-04	-479.57	0.03
4s6d ¹ D ₂	4s5p ³ P ₁	1185.525	9.629E-04	9.650E-04	-0.22	0.47
4s6d ¹ D ₂	4s5p ³ P ₂	1188.395	2.516E-05	3.142E-05	-24.89	0.01
4s6d ¹ D ₂	4s5p ¹ P ₁	1210.916	5.046E-02	5.069E-02	-0.45	24.53
4s6d ¹ D ₂	3d4p ³ D ₁	1471.142	2.112E-06	2.190E-06	-3.69	0.00
4s6d ¹ D ₂	3d4p ³ D ₂	1476.950	6.605E-06	6.655E-06	-0.75	0.00
4s6d ¹ D ₂	3d4p ³ D ₃	1485.727	6.257E-06	7.255E-06	-15.94	0.00
4s6d ¹ D ₂	4s4p ³ P ₁	335.798	4.997E-04	5.146E-04	-2.98	0.24
4s6d ¹ D ₂	3d4p ³ P ₁	1768.500	6.652E-08	9.571E-08	-43.88	0.00
4s6d ¹ D ₂	3d4p ³ P ₂	1769.990	3.555E-08	2.483E-08	30.16	0.00
4s6d ¹ D ₂	3d4p ¹ F ₃	2246.212	1.202E-03	1.889E-03	-57.15	0.58
4s6d ¹ D ₂	4s6p ¹ P ₁	3020.400	7.402E-03	9.236E-03	-24.76	3.60
4s6d ¹ D ₂	4s4f ³ F ₂	3546.577	2.016E-09	1.129E-11	99.44	0.00
4s6d ¹ D ₂	4s4f ³ F ₃	3547.017	2.270E-08	1.627E-09	92.83	0.00
4s6d ¹ D ₂	4s4p ³ P ₂	336.997	1.545E-04	1.594E-04	-3.17	0.08
4s6d ¹ D ₂	4s4f ¹ F ₃	3778.947	3.857E-06	2.326E-05	-502.93	0.00
4s6d ¹ D ₂	4s6p ³ P ₁	4046.748	1.297E-05	1.768E-05	-36.33	0.01
4s6d ¹ D ₂	4s6p ³ P ₂	4059.694	4.392E-06	5.752E-06	-30.98	0.00
4s6d ¹ D ₂	4snp ¹ P ₁	9466.559	2.409E-03	4.866E-03	-102.02	1.17
4s6d ¹ D ₂	4s5f ³ F ₂	44012.147	1.136E-08	5.438E-09	52.12	0.00

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Table 4 (continued)

Transition		λ (nm)	A_{if} (10^8 s $^{-1}$)		Diff. (%)	BR. (%)
Initial	Final		L	V		
4s6d 1D_2	4s5f 3F_3	44054.804	9.300E-08	4.405E-08	52.63	0.00
4s6d 1D_2	4s5f 1F_3	54068.667	3.250E-05	1.512E-05	53.47	0.02
4s6d 1D_2	4s7p 3P_1	310848.617	2.924E-10	1.492E-11	94.90	0.00
4s6d 1D_2	4s7p 3P_2	356252.227	4.427E-11	1.051E-12	97.63	0.00
4s6d 1D_2	4s4p 1P_1	468.658	5.757E-02			69.25
4s6d 3D_1	3d4p 3F_2	1073.120	3.603E-03	4.349E-03	-20.72	0.95
4s6d 3D_1	3d4p 1D_2	1085.345	1.577E-03	1.884E-03	-19.46	0.42
4s6d 3D_1	4s5p 3P_0	1176.280	2.879E-02	2.872E-02	0.24	7.62
4s6d 3D_1	4s5p 3P_1	1177.257	2.135E-02	2.131E-02	0.22	5.65
4s6d 3D_1	4s5p 3P_2	1180.087	1.379E-03	1.372E-03	0.53	0.36
4s6d 3D_1	4s5p 1P_1	1202.292	2.353E-04	2.346E-04	0.26	0.06
4s6d 3D_1	4s4p 3P_0	334.547	1.707E-01	1.759E-01	-3.04	45.16
4s6d 3D_1	3d4p 3D_1	1458.432	2.695E-03	2.616E-03	2.94	0.71
4s6d 3D_1	3d4p 3D_2	1464.140	9.003E-04	8.734E-04	2.99	0.24
4s6d 3D_1	3d4p 3P_0	1749.570	7.835E-05	1.128E-04	-44.03	0.02
4s6d 3D_1	4s4p 3P_1	335.132	1.280E-01	1.319E-01	-3.03	33.86
4s6d 3D_1	3d4p 3P_1	1750.164	4.797E-05	7.106E-05	-48.13	0.01
4s6d 3D_1	3d4p 3P_2	1751.623	1.974E-06	3.170E-06	-60.57	0.00
4s6d 3D_1	4s6p 1P_1	2967.306	3.408E-09	2.205E-10	93.53	0.00
4s6d 3D_1	4s4f 3F_2	3473.597	4.555E-07	5.349E-06	-1074.42	0.00
4s6d 3D_1	4s4p 3P_2	336.325	8.498E-03	8.754E-03	-3.01	2.25
4s6d 3D_1	4s6p 3P_0	3945.987	5.568E-03	7.494E-03	-34.58	1.47
4s6d 3D_1	4s6p 3P_1	3952.007	4.186E-03	5.630E-03	-34.50	1.11
4s6d 3D_1	4s6p 3P_2	3964.353	2.794E-04	3.753E-04	-34.34	0.07
4s6d 3D_1	4snp 1P_1	8963.867	3.648E-08	6.193E-08	-69.79	0.00
4s6d 3D_1	4s5f 3F_2	34910.106	1.213E-04	6.145E-05	49.33	0.03
4s6d 3D_1	4s7p 3P_0	107066.381	2.278E-06	4.384E-07	80.75	0.00
4s6d 3D_1	4s7p 3P_1	109397.221	1.601E-06	2.851E-07	82.18	0.00
4s6d 3D_1	4s7p 3P_2	114534.418	9.254E-08	1.398E-08	84.89	0.00
4s6d 3D_1	4s4p 1P_1	467.360	3.252E-06	3.641E-06	-11.96	0.00
4s6d 3D_2	3d4p 3F_2	1072.965	5.600E-04	6.729E-04	-20.16	0.15
4s6d 3D_2	3d4p 3F_3	1083.223	4.395E-03	5.317E-03	-20.97	1.17
4s6d 3D_2	3d4p 1D_2	1085.186	2.603E-05	3.473E-05	-33.42	0.01
4s6d 3D_2	4s5p 3P_1	1177.070	3.799E-02	3.790E-02	0.26	10.08
4s6d 3D_2	4s5p 3P_2	1179.899	1.291E-02	1.289E-02	0.21	3.43
4s6d 3D_2	4s5p 1P_1	1202.096	8.279E-04	8.295E-04	-0.19	0.22
4s6d 3D_2	3d4p 3D_1	1458.145	4.962E-04	4.780E-04	3.67	0.13
4s6d 3D_2	3d4p 3D_2	1463.850	2.428E-03	2.353E-03	3.08	0.64
4s6d 3D_2	3d4p 3D_3	1472.472	5.408E-04	5.232E-04	3.26	0.14
4s6d 3D_2	4s4p 3P_1	335.117	2.294E-01	2.365E-01	-3.06	60.89
4s6d 3D_2	3d4p 3P_1	1749.751	1.170E-04	1.661E-04	-41.91	0.03
4s6d 3D_2	3d4p 3P_2	1751.209	2.603E-05	3.915E-05	-50.36	0.01
4s6d 3D_2	3d4p 1F_3	2216.052	1.595E-06	2.762E-06	-73.16	0.00
4s6d 3D_2	4s6p 1P_1	2966.118	1.247E-05	1.536E-05	-23.22	0.00
4s6d 3D_2	4s4f 3F_2	3471.969	3.633E-08	6.501E-07	-1689.24	0.00
4s6d 3D_2	4s4f 3F_3	3472.391	2.941E-07	5.183E-06	-1662.09	0.00
4s6d 3D_2	4s4p 3P_2	336.310	7.651E-02	7.884E-02	-3.04	20.31
4s6d 3D_2	4s4f 1F_3	3694.358	1.691E-11	8.874E-08		0.00
4s6d 3D_2	4s6p 3P_1	3949.899	7.509E-03	1.011E-02	-34.60	1.99
4s6d 3D_2	4s6p 3P_2	3962.232	2.517E-03	3.383E-03	-34.43	0.67
4s6d 3D_2	4snp 1P_1	8953.032	5.585E-06	1.077E-05	-92.89	0.00
4s6d 3D_2	4s5f 3F_2	34746.352	1.366E-05	6.933E-06	49.23	0.00
4s6d 3D_2	4s5f 3F_3	34772.933	1.088E-04	5.521E-05	49.23	0.03
4s6d 3D_2	4s5f 1F_3	40726.562	1.239E-07	6.247E-08	49.57	0.00
4s6d 3D_2	4s7p 3P_1	107805.088	3.007E-06	5.644E-07	81.23	0.00
4s6d 3D_2	4s7p 3P_2	112790.435	8.756E-07	1.398E-07	84.03	0.00
4s6d 3D_2	4s4p 1P_1	467.331	3.448E-04	3.640E-04	-5.57	0.09
4s6d 3D_3	3d4p 3F_2	1072.740	3.034E-06	1.988E-06	34.49	0.00
4s6d 3D_3	3d4p 3F_3	1082.994	4.090E-04	4.943E-04	-20.86	0.11
4s6d 3D_3	3d4p 1D_2	1084.956	2.059E-04	2.089E-04	-1.46	0.05
4s6d 3D_3	3d4p 3F_4	1092.242	4.385E-03	5.331E-03	-21.58	1.17
4s6d 3D_3	4s5p 3P_2	1179.628	5.147E-02	5.134E-02	0.25	13.70
4s6d 3D_3	3d4p 3D_2	1463.432	3.365E-04	3.216E-04	4.42	0.09
4s6d 3D_3	3d4p 3D_3	1472.049	2.951E-03	2.848E-03	3.46	0.79
4s6d 3D_3	3d4p 3P_2	1750.611	1.644E-04	2.315E-04	-40.83	0.04
4s6d 3D_3	3d4p 1F_3	2215.095	1.731E-07	1.819E-07	-5.07	0.00
4s6d 3D_3	4s4f 3F_2	3469.620	4.376E-10	1.488E-08	-3300.03	0.00
4s6d 3D_3	4s4f 3F_3	3470.041	1.504E-08	5.199E-07	-3357.32	0.00
4s6d 3D_3	4s4p 3P_2	336.288	3.055E-01	3.149E-01	-3.10	81.33
4s6d 3D_3	4s4f 3F_4	3470.607	1.790E-07	6.017E-06	-3261.02	0.00
4s6d 3D_3	4s4f 1F_3	3691.699	5.711E-09	6.355E-09	-11.27	0.00

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Table 4 (continued)

Transition		λ (nm)	A_{if} (10^8 s^{-1})		Diff. (%)	BR. (%)
Initial	Final		L	V		
$4s6d \ ^3D_3$	$4s6p \ ^3P_2$	3959.173	1.005E-02	1.353E-02	-34.57	2.68
$4s6d \ ^3D_3$	$4s5f \ ^3F_2$	34512.511	2.834E-07	1.443E-07	49.09	0.00
$4s6d \ ^3D_3$	$4s5f \ ^3F_3$	34538.735	9.918E-06	5.048E-06	49.10	0.00
$4s6d \ ^3D_3$	$4s5f \ ^3F_4$	34572.169	1.145E-04	5.826E-05	49.11	0.03
$4s6d \ ^3D_3$	$4s5f \ ^1F_3$	40405.673	1.512E-12	1.608E-13	89.36	0.00
$4s6d \ ^3D_3$	$4s7p \ ^3P_2$	110363.095	3.748E-06	6.449E-07	82.79	0.00

Table 5
Spontaneous emission rates of transitions originating from the $4snf$ ($n = 4-6$) states of Ca I.

Transition		λ (nm)	$A_{if}(10^8 \text{ s}^{-1})$		Diff. (%)	BR. (%)
Initial	Final		L	V		
4s4f 3F_2	4s5s 3S_1	940.671	2.802E-13	1.357E-13	51.58	0.00
4s4f 3F_2	4s4d 1D_2	2052.579	1.385E-06	1.352E-06	2.37	0.00
4s4f 3F_2	4s4d 3D_1	2261.415	8.393E-02	8.413E-02	-0.23	32.22
4s4f 3F_2	4s4d 3D_2	2263.293	1.559E-02	1.562E-02	-0.21	5.98
4s4f 3F_2	4s4d 3D_3	2266.155	4.422E-04	4.429E-04	-0.18	0.17
4s4f 3F_2	4p 2 3P_1	2698.764	2.194E-06	2.208E-06	-0.60	0.00
4s4f 3F_2	4p 2 3P_2	2763.462	6.099E-07	6.172E-07	-1.21	0.00
4s4f 3F_2	4s6s 3S_1	5896.331	2.241E-13	2.165E-13	3.39	0.00
4s4f 3F_2	4p 2 1D_2	6894.840	3.576E-09	4.377E-09	-22.40	0.00
4s4f 3F_2	3d4s 3D_1	457.983	1.348E-01	1.346E-01	0.12	51.72
4s4f 3F_2	3d4s 3D_2	458.275	2.508E-02	2.506E-02	0.11	9.63
4s4f 3F_2	3d4s 3D_3	458.732	7.142E-04	7.134E-04	0.11	0.27
4s4f 3F_2	3d4s 1D_2	492.112	9.191E-06	9.248E-06	-0.62	0.00
4s4f 3F_3	4s4d 1D_2	2052.431	1.173E-05	1.187E-05	-1.17	0.00
4s4f 3F_3	4s4d 3D_2	2263.114	8.863E-02	8.885E-02	-0.24	34.02
4s4f 3F_3	4s4d 3D_3	2265.976	1.106E-02	1.108E-02	-0.22	4.24
4s4f 3F_3	4p 2 3P_2	2763.194	3.435E-06	3.449E-06	-0.39	0.00
4s4f 3F_3	4p 2 1D_2	6893.176	4.241E-09	3.877E-09	8.59	0.00
4s4f 3F_3	3d4s 3D_2	458.268	1.429E-01	1.427E-01	0.12	54.84
4s4f 3F_3	3d4s 3D_3	458.725	1.791E-02	1.789E-02	0.11	6.87
4s4f 3F_3	3d4s 1D_2	492.103	3.396E-05	3.360E-05	1.07	0.01
4s4f 3F_4	4s4d 3D_3	2265.734	9.963E-02	9.990E-02	-0.26	38.13
4s4f 3F_4	3d4s 3D_3	458.715	1.617E-01	1.615E-01	0.13	61.87
4s4f 1F_3	4s4d 1D_2	1982.043	6.368E-02	6.694E-02	-5.12	16.83
4s4f 1F_3	4s4d 3D_2	2177.833	4.902E-06	5.192E-06	-5.92	0.00
4s4f 1F_3	4s4d 3D_3	2180.483	6.505E-08	5.181E-08	20.35	0.00
4s4f 1F_3	4p 2 3P_2	2637.110	2.345E-05	2.319E-05	1.10	0.01
4s4f 1F_3	4p 2 1D_2	6158.621	2.920E-03	2.690E-03	7.88	0.77
4s4f 1F_3	3d4s 3D_2	454.663	5.336E-05	4.883E-05	8.49	0.01
4s4f 1F_3	3d4s 3D_3	455.112	1.616E-05	1.754E-05	-8.50	0.00
4s4f 1F_3	3d4s 1D_2	487.949	3.116E-01	2.919E-01	6.32	82.37
4s5f 3F_2	4s5s 3S_1	756.251	4.042E-13	2.396E-13	40.73	0.00
4s5f 3F_2	4s4d 1D_2	1339.705	2.099E-07	1.973E-07	6.00	0.00
4s5f 3F_2	4s4d 3D_1	1425.635	1.131E-02	1.132E-02	-0.08	6.65
4s5f 3F_2	4s4d 3D_2	1426.381	2.086E-03	2.087E-03	-0.03	1.23
4s5f 3F_2	4s4d 3D_3	1427.517	5.888E-05	5.885E-05	0.06	0.03
4s5f 3F_2	4p 2 3P_1	1587.854	4.242E-08	4.323E-08	-1.91	0.00
4s5f 3F_2	4p 2 3P_2	1610.031	7.211E-09	7.895E-09	-9.48	0.00
4s5f 3F_2	4s6s 3S_1	2331.883	1.295E-12	1.288E-12	0.51	0.00
4s5f 3F_2	4p 2 1D_2	2473.552	1.699E-08	1.574E-08	7.38	0.00
4s5f 3F_2	4s5d 3D_1	4951.427	2.095E-02	2.217E-02	-5.80	12.31
4s5f 3F_2	4s5d 3D_2	4955.647	3.886E-03	4.110E-03	-5.78	2.28
4s5f 3F_2	4s5d 3D_3	4962.213	1.106E-04	1.170E-04	-5.78	0.06
4s5f 3F_2	4s5d 1D_2	5424.258	5.316E-07	5.810E-07	-9.30	0.00
4s5f 3F_2	3d 2 3F_2	7765.241	3.178E-08	5.672E-07	-1684.76	0.00
4s5f 3F_2	3d4s 3D_1	409.379	1.106E-01	1.122E-01	-1.51	64.99
4s5f 3F_2	3d 2 3F_3	7852.375	4.424E-09	7.138E-08	-1513.46	0.00
4s5f 3F_2	4s7s 3S_1	12790.177	2.412E-14	3.985E-14	-65.24	0.00
4s5f 3F_2	3d4s 3D_2	409.612	2.057E-02	2.088E-02	-1.51	12.09
4s5f 3F_2	3d4s 3D_3	409.977	5.884E-04	5.973E-04	-1.50	0.35
4s5f 3F_2	3d4s 1D_2	436.434	6.474E-06	6.582E-06	-1.66	0.00
4s5f 3F_3	4s4d 1D_2	1339.665	1.773E-06	1.806E-06	-1.85	0.00
4s5f 3F_3	4s4d 3D_2	1426.336	1.192E-02	1.193E-02	-0.12	7.00
4s5f 3F_3	4s4d 3D_3	1427.472	1.475E-03	1.476E-03	-0.03	0.87
4s5f 3F_3	4p 2 3P_2	1609.974	4.163E-08	4.164E-08	-0.03	0.00
4s5f 3F_3	4p 2 1D_2	2473.417	5.270E-08	5.376E-08	-2.01	0.00
4s5f 3F_3	4s5d 3D_2	4955.107	2.214E-02	2.342E-02	-5.80	13.01
4s5f 3F_3	4s5d 3D_3	4961.671	2.764E-03	2.925E-03	-5.80	1.62
4s5f 3F_3	4s5d 1D_2	5423.611	2.734E-06	2.905E-06	-6.27	0.00
4s5f 3F_3	3d 2 3F_2	7763.915	3.583E-09	4.521E-08	-1161.85	0.00
4s5f 3F_3	3d 2 3F_3	7851.019	2.904E-08	5.463E-07	-1781.01	0.00
4s5f 3F_3	3d 2 3F_4	7969.715	3.279E-09	5.241E-08	-1498.50	0.00
4s5f 3F_3	3d4s 3D_2	409.608	1.172E-01	1.189E-01	-1.50	68.84
4s5f 3F_3	3d4s 3D_3	409.973	1.471E-02	1.493E-02	-1.50	8.64
4s5f 3F_3	3d4s 1D_2	436.429	3.280E-05	3.278E-05	0.06	0.02
4s5f 3F_4	4s4d 3D_3	1427.415	1.333E-02	1.335E-02	-0.14	7.82
4s5f 3F_4	4s5d 3D_3	4960.982	2.489E-02	2.634E-02	-5.82	14.59
4s5f 3F_4	3d 2 3F_3	7849.294	3.028E-09	3.428E-08	-1031.94	0.00
4s5f 3F_4	3d 2 3F_4	7967.937	3.248E-08	6.179E-07	-1802.55	0.00
4s5f 3F_4	3d4s 3D_3	409.968	1.323E-01	1.343E-01	-1.51	77.59

(continued on next page)

Table 5 (continued)

Transition		λ (nm)	$A_{if}(10^8 \text{ s}^{-1})$		Diff. (%)	BR. (%)
Initial	Final		L	V		
4s5f ¹ F ₃	4s4d ¹ D ₂	1332.163	1.783E-02	1.829E-02	-2.58	7.72
4s5f ¹ F ₃	4s4d ³ D ₂	1417.834	7.599E-07	7.848E-07	-3.28	0.00
4s5f ¹ F ₃	4s4d ³ D ₃	1418.957	2.190E-10	9.774E-11	55.36	0.00
4s5f ¹ F ₃	4p ² ³ P ₂	1599.151	9.537E-07	9.462E-07	0.78	0.00
4s5f ¹ F ₃	4p ² ¹ D ₂	2447.962	5.935E-03	6.158E-03	-3.76	2.57
4s5f ¹ F ₃	4s5d ³ D ₂	4853.992	2.822E-06	3.029E-06	-7.36	0.00
4s5f ¹ F ₃	4s5d ³ D ₃	4860.291	1.191E-09	8.065E-10	32.30	0.00
4s5f ¹ F ₃	4s5d ¹ D ₂	5302.705	1.878E-02	2.032E-02	-8.20	8.13
4s5f ¹ F ₃	3d ² ³ F ₂	7518.514	4.818E-07	5.906E-07	-22.59	0.00
4s5f ¹ F ₃	3d ² ³ F ₃	7600.170	1.378E-10	1.242E-09	-801.12	0.00
4s5f ¹ F ₃	3d ² ³ F ₄	7711.349	1.617E-10	7.512E-10	-364.55	0.00
4s5f ¹ F ₃	3d4s ³ D ₂	408.904	3.547E-05	3.541E-05	0.17	0.02
4s5f ¹ F ₃	3d4s ³ D ₃	409.268	3.427E-07	3.977E-07	-16.05	0.00
4s5f ¹ F ₃	3d4s ¹ D ₂	435.630	1.884E-01	1.866E-01	0.95	81.57
4s6f ³ F ₂	4s5s ³ S ₁	23476.383	3.096E-11			0.00
4s6f ³ F ₂	4s4d ¹ D ₂	683.754	7.751E-09			0.00
4s6f ³ F ₂	4s4d ³ D ₁	1127.860	2.663E-03			3.00
4s6f ³ F ₂	4s4d ³ D ₂	1188.151	4.872E-04			0.55
4s6f ³ F ₂	4s4d ³ D ₃	1188.669	1.364E-05			0.02
4s6f ³ F ₂	4p ² ³ P ₁	1189.458	1.919E-07			0.00
4s6f ³ F ₂	4p ² ³ P ₂	1298.730	2.903E-08			0.00
4s6f ³ F ₂	4s6s ³ S ₁	1313.529	6.059E-13			0.00
4s6f ³ F ₂	4p ² ¹ D ₂	1757.346	1.426E-08			0.00
4s6f ³ F ₂	4s5d ³ D ₁	1836.618	6.585E-03			7.42
4s6f ³ F ₂	4s5d ³ D ₂	2922.575	1.215E-03			1.37
4s6f ³ F ₂	4s5d ³ D ₃	2924.045	3.456E-05			0.04
4s6f ³ F ₂	4s5d ¹ D ₂	2926.330	4.574E-07			0.00
4s6f ³ F ₂	3d ² ³ F ₂	3081.104	5.369E-07			0.00
4s6f ³ F ₂	3d ² ³ F ₃	3717.735	6.821E-08			0.00
4s6f ³ F ₂	4s7s ³ S ₁	387.158	5.704E-14			0.00
4s6f ³ F ₂	3d4s ³ D ₁	3737.591	5.931E-02			66.82
4s6f ³ F ₂	3d4s ³ D ₂	4579.027	1.101E-02			12.40
4s6f ³ F ₂	4s6d ¹ D ₂	387.366	1.013E-06			0.00
4s6f ³ F ₂	4s6d ³ D ₁	8512.015	5.860E-03			6.60
4s6f ³ F ₂	4s6d ³ D ₂	8964.027	1.089E-03			1.23
4s6f ³ F ₂	4s6d ³ D ₃	8974.888	1.648E-04			0.19
4s6f ³ F ₂	4s8s ³ S ₁	8990.623	1.511E-12			0.00
4s6f ³ F ₂	3d4s ³ D ₃	387.692	3.166E-04			0.36
4s6f ³ F ₂	3d4s ¹ D ₂	411.269	1.067E-05			0.01
4s6f ³ F ₃	4s4d ¹ D ₂	1127.841	7.618E-08			0.00
4s6f ³ F ₃	4s4d ³ D ₂	1188.648	2.806E-03			3.19
4s6f ³ F ₃	4s4d ³ D ₃	1189.437	3.444E-04			0.39
4s6f ³ F ₃	4p ² ³ P ₂	1313.503	1.671E-07			0.00
4s6f ³ F ₃	4p ² ¹ D ₂	1836.568	1.285E-07			0.00
4s6f ³ F ₃	4s5d ³ D ₂	2923.917	6.950E-03			7.90
4s6f ³ F ₃	4s5d ³ D ₃	2926.201	8.652E-04			0.98
4s6f ³ F ₃	4s5d ¹ D ₂	3080.962	4.168E-06			0.00
4s6f ³ F ₃	3d ² ³ F ₂	3717.527	1.031E-08			0.00
4s6f ³ F ₃	3d ² ³ F ₃	3737.382	4.362E-07			0.00
4s6f ³ F ₃	3d ² ³ F ₄	3764.068	4.538E-08			0.00
4s6f ³ F ₃	4s5g ¹ G ₄	387.364	5.031E-10			0.00
4s6f ³ F ₃	4s6d ¹ D ₂	7758.915	4.900E-06			0.01
4s6f ³ F ₃	3d4s ³ D ₂	8510.928	6.277E-02			71.37
4s6f ³ F ₃	4s6d ³ D ₂	8973.680	6.224E-03			7.08
4s6f ³ F ₃	4s6d ³ D ₃	8989.410	1.029E-05			0.01
4s6f ³ F ₃	3d4s ³ D ₃	387.690	7.898E-03			8.98
4s6f ³ F ₃	3d4s ¹ D ₂	411.266	7.556E-05			0.09
4s6f ³ F ₄	4s4d ³ D ₃	1189.411	3.132E-03			3.82
4s6f ³ F ₄	4s5d ³ D ₃	2926.047	7.799E-03			9.50
4s6f ³ F ₄	3d ² ³ F ₃	3737.130	3.533E-08			0.00
4s6f ³ F ₄	3d ² ³ F ₄	3763.813	4.728E-07			0.00
4s6f ³ F ₄	4s5g ³ G ₅	7751.277	2.433E-04			0.30
4s6f ³ F ₄	4s5g ¹ G ₄	7757.832	6.584E-12			0.00
4s6f ³ F ₄	4s6d ³ D ₃	8987.956	1.238E-07			0.00
4s6f ³ F ₄	3d4s ³ D ₃	387.688	7.088E-02			86.38
4s6f ¹ F ₃	4s4d ¹ D ₂	1125.605	5.391E-03			5.21
4s6f ¹ F ₃	4s4d ³ D ₂	1186.165	1.504E-11			0.00
4s6f ¹ F ₃	4s4d ³ D ₃	1186.951	1.325E-08			0.00
4s6f ¹ F ₃	4p ² ³ P ₂	1310.472	3.967E-07			0.00
4s6f ¹ F ₃	4p ² ¹ D ₂	1830.647	2.969E-03			2.87
4s6f ¹ F ₃	4s5d ³ D ₂	2908.939	5.057E-06			0.00

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Table 5 (continued)

Transition		λ (nm)	$A_{if}(10^8 \text{ s}^{-1})$		Diff. (%)	BR. (%)
Initial	Final		L	V		
4s6f 1F_3	4s5d 3D_3	2911.200	7.052E-09			0.00
4s6f 1F_3	4s5d 1D_2	3064.336	5.037E-03			4.87
4s6f 1F_3	3d 2 3F_2	3693.349	2.889E-05			0.03
4s6f 1F_3	3d 2 3F_3	3712.945	3.051E-10			0.00
4s6f 1F_3	3d 2 3F_4	3739.282	1.498E-09			0.00
4s6f 1F_3	4s5g 1G_4	387.100	7.996E-05			0.08
4s6f 1F_3	4s6d 1D_2	7654.330	5.901E-03			5.71
4s6f 1F_3	4s6d 3D_2	8385.252	6.309E-06			0.01
4s6f 1F_3	4s6d 3D_3	8834.078	6.540E-11			0.00
4s6f 1F_3	3d4s 3D_2	8849.323	9.069E-05			0.09
4s6f 1F_3	3d4s 3D_3	387.426	7.248E-08			0.00
4s6f 1F_3	3d4s 1D_2	410.968	8.390E-02			81.13

Table 6
Spontaneous emission rates of transitions originating from the $3d^2$, $4p^2$, $3d4p$, and $4s5g$ states of Ca I.

Transition		λ (nm)	$A_{if}(10^8 \text{ s}^{-1})$		Diff. (%)	BR. (%)
Initial	Final		L	V		
$3d4p^3F_2$	$4s5s^3S_1$	2386.094	1.489E-05	1.490E-05	-0.06	0.00
$3d4p^3F_2$	$3d4s^3D_1$	649.558	2.250E-01	2.062E-01	8.37	56.13
$3d4p^3F_2$	$3d4s^3D_2$	650.145	4.840E-02	4.514E-02	6.74	12.07
$3d4p^3F_2$	$3d4s^3D_3$	651.065	7.591E-04	6.482E-04	14.60	0.19
$3d4p^3F_2$	$3d4s^1D_2$	720.419	1.267E-01	1.435E-01	-13.25	31.61
$3d4p^3F_3$	$3d4s^3D_2$	646.435	3.367E-01	3.086E-01	8.36	88.32
$3d4p^3F_3$	$3d4s^3D_3$	647.345	4.447E-02	4.113E-02	7.51	11.67
$3d4p^3F_3$	$3d4s^1D_2$	715.867	5.039E-05	4.493E-05	10.83	0.01
$3d4p^1D_2$	$4s5s^3S_1$	2327.796	1.115E-04	1.118E-04	-0.28	0.02
$3d4p^1D_2$	$3d4s^3D_1$	645.159	9.127E-02	8.382E-02	8.16	20.46
$3d4p^1D_2$	$3d4s^3D_2$	645.738	1.210E-02	1.073E-02	11.31	2.71
$3d4p^1D_2$	$3d4s^3D_3$	646.646	1.798E-03	1.857E-03	-3.30	0.40
$3d4p^1D_2$	$3d4s^1D_2$	715.012	3.408E-01	3.840E-01	-12.67	76.40
$3d4p^3F_4$	$3d4s^3D_3$	644.085	3.850E-01	3.530E-01	8.30	100.00
$3d4p^3D_1$	$4s5s^3S_1$	1503.106	2.929E-06	2.599E-06	11.27	0.00
$3d4p^3D_1$	$4s^2^1S_0$	261.832	7.250E-05	9.235E-05	-27.38	0.01
$3d4p^3D_1$	$4s5s^1S_0$	2051.227	8.697E-06	9.073E-06	-4.33	0.00
$3d4p^3D_1$	$4s4d^1D_2$	11184.431	1.313E-07	1.517E-07	-15.48	0.00
$3d4p^3D_1$	$4s4d^3D_1$	22512.889	4.675E-07	8.653E-07	-85.10	0.00
$3d4p^3D_1$	$4s4d^3D_2$	22700.445	2.167E-07	3.977E-07	-83.57	0.00
$3d4p^3D_1$	$3d4s^3D_1$	560.004	5.100E-01	5.685E-01	-11.48	74.03
$3d4p^3D_1$	$3d4s^3D_2$	560.440	1.788E-01	2.002E-01	-12.00	25.95
$3d4p^3D_1$	$3d4s^1D_2$	611.892	1.973E-05	1.650E-05	16.35	0.00
$3d4p^3D_2$	$4s5s^3S_1$	1497.091	5.606E-06	5.337E-06	4.80	0.00
$3d4p^3D_2$	$4s4d^1D_2$	10859.768	9.848E-11	6.034E-10	-512.78	0.00
$3d4p^3D_2$	$4s4d^3D_1$	21235.029	1.139E-07	2.015E-07	-76.85	0.00
$3d4p^3D_2$	$4s4d^3D_2$	21401.819	4.939E-07	9.157E-07	-85.39	0.00
$3d4p^3D_2$	$4s4d^3D_3$	21660.493	1.881E-07	3.420E-07	-81.77	0.00
$3d4p^3D_2$	$3d4s^3D_1$	559.167	1.062E-01	1.181E-01	-11.22	15.39
$3d4p^3D_2$	$3d4s^3D_2$	559.601	4.691E-01	5.232E-01	-11.51	67.98
$3d4p^3D_2$	$3d4s^3D_3$	560.283	1.146E-01	1.288E-01	-12.37	16.61
$3d4p^3D_2$	$3d4s^1D_2$	610.893	1.438E-04	1.689E-04	-17.46	0.02
$3d4p^3D_3$	$4s4d^1D_2$	10407.668	3.897E-08	2.840E-08	27.12	0.00
$3d4p^3D_3$	$4s4d^3D_2$	19714.145	1.103E-07	1.898E-07	-72.05	0.00
$3d4p^3D_3$	$4s4d^3D_3$	19933.422	8.589E-07	1.569E-06	-82.62	0.00
$3d4p^3D_3$	$3d4s^3D_2$	558.352	8.072E-02	8.971E-02	-11.14	11.66
$3d4p^3D_3$	$3d4s^3D_3$	559.030	6.113E-01	6.825E-01	-11.65	88.33
$3d4p^3D_3$	$3d4s^1D_2$	609.403	1.765E-07	8.340E-07	-372.51	0.00
$4p^2^3P_0$	$4s5p^3P_1$	5368.292	6.316E-07	3.988E-06	-531.44	0.00
$4p^2^3P_0$	$4s5p^1P_1$	5931.480	6.195E-07	5.585E-07	9.85	0.00
$4p^2^3P_0$	$3d4p^3D_1$	44414.835	3.804E-07	1.233E-06	-224.19	0.00
$4p^2^3P_0$	$4s4p^3P_1$	430.896	1.826E+00	2.020E+00	-10.65	99.98
$4p^2^3P_0$	$4s4p^1P_1$	677.266	2.992E-04	3.512E-04	-17.40	0.02
$4p^2^3P_1$	$3d4p^3F_2$	3657.163	1.577E-08	8.457E-09	46.38	0.00
$4p^2^3P_1$	$3d4p^1D_2$	3803.149	6.818E-09	2.776E-09	59.28	0.00
$4p^2^3P_1$	$4s5p^3P_0$	5216.158	1.346E-06	3.461E-06	-157.02	0.00
$4p^2^3P_1$	$4s5p^3P_1$	5235.438	2.798E-07	1.248E-06	-345.96	0.00
$4p^2^3P_1$	$4s5p^3P_2$	5291.873	1.654E-09	6.758E-07	-0.00	0.00
$4p^2^3P_1$	$4s5p^1P_1$	5769.708	1.410E-09	6.768E-10	51.99	0.00
$4p^2^3P_1$	$4s4p^3P_0$	429.057	6.116E-01	6.765E-01	-10.62	33.42
$4p^2^3P_1$	$3d4p^3D_1$	36708.024	1.646E-07	7.103E-07	-331.44	0.00
$4p^2^3P_1$	$3d4p^3D_2$	40701.697	3.709E-07	1.379E-06	-271.81	0.00
$4p^2^3P_1$	$4s4p^3P_1$	430.020	4.633E-01	5.123E-01	-10.56	25.32
$4p^2^3P_1$	$4s4p^3P_2$	431.987	7.551E-01	8.358E-01	-10.69	41.26
$4p^2^3P_1$	$4s4p^1P_1$	675.105	4.708E-06	6.010E-06	-27.64	0.00
$4p^2^3P_2$	$3d4p^3F_2$	3544.704	2.188E-08	7.096E-08	-224.26	0.00
$4p^2^3P_2$	$3d4p^3F_3$	3659.184	4.339E-08	1.008E-08	76.78	0.00
$4p^2^3P_2$	$3d4p^1D_2$	3681.682	1.422E-07	2.910E-07	-104.66	0.00
$4p^2^3P_2$	$4s5p^3P_1$	5007.988	9.858E-07	2.596E-06	-163.32	0.00
$4p^2^3P_2$	$4s5p^3P_2$	5059.602	3.420E-07	2.677E-06	-682.95	0.00
$4p^2^3P_2$	$4s5p^1P_1$	5494.687	2.137E-06	2.192E-06	-2.59	0.00
$4p^2^3P_2$	$3d4p^3D_1$	27841.969	1.472E-08	1.770E-07	-1102.26	0.00
$4p^2^3P_2$	$3d4p^3D_2$	30080.616	1.749E-07	1.156E-06	-560.76	0.00
$4p^2^3P_2$	$3d4p^3D_3$	34195.049	6.898E-07	3.349E-06	-385.57	0.00
$4p^2^3P_2$	$4s4p^3P_1$	428.421	4.571E-01	5.055E-01	-10.59	24.93
$4p^2^3P_2$	$4s4p^3P_2$	430.374	1.376E+00	1.522E+00	-10.59	75.05
$4p^2^3P_2$	$4s4p^1P_1$	671.174	3.911E-04	4.160E-04	-6.39	0.02
$3d4p^3P_0$	$4s5s^3S_1$	1283.058	5.926E-03	5.734E-03	3.24	0.76
$3d4p^3P_0$	$4s4d^3D_1$	6308.432	7.123E-04	9.429E-04	-32.38	0.09

(continued on next page)

Table 6 (continued)

Transition		λ (nm)	A_{if} (10^8 s^{-1})		Diff. (%)	BR. (%)
Initial	Final		L	V		
3d4p ³ P ₀	4p ² ³ P ₁	11513.177	1.430E-07	1.807E-06	-1163.46	0.00
3d4p ³ P ₀	3d4s ³ D ₁	526.371	7.748E-01	9.561E-01	-23.40	99.15
3d4p ³ P ₁	4s5s ³ S ₁	1282.739	5.936E-03	5.734E-03	3.41	0.76
3d4p ³ P ₁	4s ² ¹ S ₀	254.224	8.447E-05	9.012E-05	-6.69	0.01
3d4p ³ P ₁	4s5s ¹ S ₀	1661.665	8.536E-06	8.572E-06	-0.42	0.00
3d4p ³ P ₁	4s4d ¹ D ₂	4909.108	1.481E-06	1.789E-06	-20.79	0.00
3d4p ³ P ₁	4s4d ³ D ₁	6300.721	1.806E-04	2.392E-04	-32.43	0.02
3d4p ³ P ₁	4s4d ³ D ₂	6315.324	5.308E-04	7.037E-04	-32.58	0.07
3d4p ³ P ₁	4p ² ³ P ₀	10895.857	9.717E-08	4.750E-07	-388.82	0.00
3d4p ³ P ₁	4p ² ³ P ₁	11487.519	4.307E-08	3.780E-07	-777.57	0.00
3d4p ³ P ₁	4p ² ³ P ₂	12759.008	5.176E-08	6.460E-07	-1148.16	0.00
3d4p ³ P ₁	3d4s ³ D ₁	526.317	2.025E-01	2.493E-01	-23.08	25.95
3d4p ³ P ₁	3d4s ³ D ₂	526.702	5.712E-01	7.062E-01	-23.63	73.18
3d4p ³ P ₁	3d4s ¹ D ₂	571.896	3.207E-05	3.961E-05	-23.51	0.00
3d4p ³ P ₂	4s5s ³ S ₁	1281.956	5.961E-03	5.754E-03	3.48	0.77
3d4p ³ P ₂	4s4d ¹ D ₂	4897.663	2.486E-10	2.697E-09	-984.62	0.00
3d4p ³ P ₂	4s4d ³ D ₁	6281.881	7.430E-06	9.849E-06	-32.55	0.00
3d4p ³ P ₂	4s4d ³ D ₂	6296.397	1.095E-04	1.451E-04	-32.59	0.01
3d4p ³ P ₂	4s4d ³ D ₃	6318.596	5.950E-04	7.906E-04	-32.87	0.08
3d4p ³ P ₂	4p ² ³ P ₁	11425.046	1.004E-07	2.588E-07	-157.78	0.00
3d4p ³ P ₂	4p ² ³ P ₂	12681.987	1.437E-07	8.985E-07	-525.27	0.00
3d4p ³ P ₂	3d4s ³ D ₁	526.185	8.820E-03	1.081E-02	-22.54	1.13
3d4p ³ P ₂	3d4s ³ D ₂	526.570	1.248E-01	1.535E-01	-23.03	16.02
3d4p ³ P ₂	3d4s ³ D ₃	527.174	6.382E-01	7.903E-01	-23.84	81.96
3d4p ³ P ₂	3d4s ¹ D ₂	571.741	2.357E-04	2.689E-04	-14.10	0.03
3d4p ¹ F ₃	4s4d ¹ D ₂	3086.801	1.565E-02	1.370E-02	12.50	21.49
3d4p ¹ F ₃	4s4d ³ D ₂	3589.350	1.096E-06	9.243E-07	15.64	0.00
3d4p ¹ F ₃	4s4d ³ D ₃	3596.553	9.869E-09	9.761E-09	1.09	0.00
3d4p ¹ F ₃	4p ² ³ P ₂	5034.410	9.118E-07	9.848E-07	-8.00	0.00
3d4p ¹ F ₃	3d4s ³ D ₂	495.328	8.657E-06	5.114E-06	40.93	0.01
3d4p ¹ F ₃	3d4s ³ D ₃	495.862	1.253E-04	1.353E-04	-7.92	0.17
3d4p ¹ F ₃	3d4s ¹ D ₂	535.095	5.705E-02	4.314E-02	24.38	78.32
4p ² ¹ D ₂	3d4p ³ F ₂	2004.249	1.011E-03	1.219E-03	-20.49	0.17
4p ² ¹ D ₂	3d4p ³ F ₃	2040.342	1.507E-07	1.511E-07	-0.27	0.00
4p ² ¹ D ₂	3d4p ¹ D ₂	2047.318	2.401E-03	2.903E-03	-20.89	0.40
4p ² ¹ D ₂	4s5p ³ P ₁	2400.903	1.333E-04	1.276E-04	4.31	0.02
4p ² ¹ D ₂	4s5p ³ P ₂	2412.702	8.136E-06	9.871E-06	-21.32	0.00
4p ² ¹ D ₂	4s5p ¹ P ₁	2507.378	1.308E-02	1.248E-02	4.60	2.20
4p ² ¹ D ₂	3d4p ³ D ₁	3956.541	1.206E-06	1.147E-06	4.90	0.00
4p ² ¹ D ₂	3d4p ³ D ₂	3998.832	3.892E-08	3.281E-08	15.68	0.00
4p ² ¹ D ₂	3d4p ³ D ₃	4063.835	4.311E-08	1.269E-08	70.57	0.00
4p ² ¹ D ₂	4s4p ³ P ₁	392.006	4.591E-05	5.303E-05	-15.51	0.01
4p ² ¹ D ₂	3d4p ³ P ₁	7222.668	1.387E-07	1.401E-07	-1.04	0.00
4p ² ¹ D ₂	3d4p ³ P ₂	7247.585	2.099E-08	7.039E-08	-235.33	0.00
4p ² ¹ D ₂	3d4p ¹ F ₃	54957.133	2.891E-07	3.722E-06	-1187.40	0.00
4p ² ¹ D ₂	4s4p ³ P ₂	393.640	7.852E-04	8.614E-04	-9.70	0.13
4p ² ¹ D ₂	4s4p ¹ P ₁	585.907	5.760E-01	6.310E-01	-9.55	97.06
4p ² ¹ S ₀	4s5p ³ P ₁	1911.487	1.158E-04	1.302E-04	-12.38	0.01
4p ² ¹ S ₀	4s5p ¹ P ₁	1978.372	1.276E-02	1.436E-02	-12.54	1.61
4p ² ¹ S ₀	3d4p ³ D ₁	2782.500	1.236E-06	1.489E-06	-20.55	0.00
4p ² ¹ S ₀	4s4p ³ P ₁	376.276	1.085E-03	1.177E-03	-8.45	0.14
4p ² ¹ S ₀	3d4p ³ P ₁	4080.034	2.225E-06	2.502E-06	-12.47	0.00
4p ² ¹ S ₀	4s6p ¹ P ₁	93222.709	2.055E-06	8.250E-07	59.85	0.00
4p ² ¹ S ₀	4s4p ¹ P ₁	551.451	7.780E-01	8.682E-01	-11.59	98.24
3d ² ³ F ₂	3d4p ³ F ₂	1291.259	2.826E-02	3.549E-02	-25.58	41.20
3d ² ³ F ₂	3d4p ³ F ₃	1306.145	4.691E-03	5.912E-03	-26.03	6.84
3d ² ³ F ₂	3d4p ¹ D ₂	1309.000	1.043E-02	1.312E-02	-25.81	15.20
3d ² ³ F ₂	4s5p ³ P ₁	1445.070	2.803E-07	2.438E-07	13.00	0.00
3d ² ³ F ₂	4s5p ³ P ₂	1449.336	2.329E-06	3.080E-06	-32.22	0.00
3d ² ³ F ₂	4s5p ¹ P ₁	1482.973	3.879E-06	3.621E-06	6.66	0.01
3d ² ³ F ₂	3d4p ³ D ₁	1893.065	2.132E-02	2.025E-02	5.02	31.08
3d ² ³ F ₂	3d4p ³ D ₂	1902.693	3.754E-03	3.547E-03	5.51	5.47
3d ² ³ F ₂	3d4p ³ D ₃	1917.285	9.916E-05	9.262E-05	6.59	0.14
3d ² ³ F ₂	4s4p ³ P ₁	353.797	9.691E-08	3.045E-08	68.57	0.00
3d ² ³ F ₂	3d4p ³ P ₁	2415.745	2.031E-06	2.003E-06	1.36	0.00
3d ² ³ F ₂	3d4p ³ P ₂	2418.526	6.890E-07	6.922E-07	-0.46	0.00
3d ² ³ F ₂	3d4p ¹ F ₃	3404.904	2.474E-07	3.775E-07	-52.57	0.00
3d ² ³ F ₂	4s6p ¹ P ₁	5568.487	2.282E-07	2.658E-07	-16.47	0.00
3d ² ³ F ₂	4s4f ³ F ₂	7665.067	1.019E-07	6.964E-07	-583.68	0.00
3d ² ³ F ₂	4s4f ³ F ₃	7667.124	1.199E-08	8.371E-08	-597.88	0.00
3d ² ³ F ₂	4s4p ³ P ₂	355.128	2.801E-09	1.007E-10	96.41	0.00

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Table 6 (continued)

Transition		λ (nm)	$A_{if}(10^8 \text{ s}^{-1})$		Diff. (%)	BR. (%)
Initial	Final		L	V		
$3d^2 \ ^3F_2$	$4s4f \ ^1F_3$	8839.857	3.297E-08	2.348E-08	28.79	0.00
$3d^2 \ ^3F_2$	$4s6p \ ^3P_1$	10458.938	1.945E-10	1.992E-10	-2.41	0.00
$3d^2 \ ^3F_2$	$4s6p \ ^3P_2$	10545.853	5.590E-11	6.354E-11	-13.65	0.00
$3d^2 \ ^3F_2$	$4s4p \ ^1P_1$	504.476	3.937E-05	4.524E-05	-14.90	0.06
$3d^2 \ ^3F_3$	$3d4p \ ^3F_2$	1288.881	2.306E-03	2.934E-03	-27.24	3.41
$3d^2 \ ^3F_3$	$3d4p \ ^3F_3$	1303.711	3.596E-02	4.524E-02	-25.80	53.17
$3d^2 \ ^3F_3$	$3d4p \ ^1D_2$	1306.556	9.782E-04	1.232E-03	-25.90	1.45
$3d^2 \ ^3F_3$	$3d4p \ ^3F_4$	1317.136	3.292E-03	4.159E-03	-26.33	4.87
$3d^2 \ ^3F_3$	$4s5p \ ^3P_2$	1446.341	1.068E-06	1.125E-06	-5.35	0.00
$3d^2 \ ^3F_3$	$3d4p \ ^3D_2$	1897.533	2.249E-02	2.136E-02	5.02	33.25
$3d^2 \ ^3F_3$	$3d4p \ ^3D_3$	1912.046	2.605E-03	2.454E-03	5.80	3.85
$3d^2 \ ^3F_3$	$3d4p \ ^3P_2$	2410.196	3.913E-06	3.858E-06	1.40	0.01
$3d^2 \ ^3F_3$	$3d4p \ ^1F_3$	3388.418	1.948E-07	1.508E-07	22.57	0.00
$3d^2 \ ^3F_3$	$4s4f \ ^3F_2$	7582.018	1.001E-08	6.587E-08	-558.24	0.00
$3d^2 \ ^3F_3$	$4s4f \ ^3F_3$	7584.031	1.028E-07	6.809E-07	-562.43	0.00
$3d^2 \ ^3F_3$	$4s4p \ ^3P_2$	354.948	1.583E-07	6.037E-08	61.86	0.00
$3d^2 \ ^3F_3$	$4s4f \ ^3F_4$	7586.735	9.143E-09	6.170E-08	-574.86	0.00
$3d^2 \ ^3F_3$	$4s4f \ ^1F_3$	8729.584	1.863E-09	4.751E-10	74.50	0.00
$3d^2 \ ^3F_3$	$4s6p \ ^3P_2$	10389.287	3.400E-10	3.393E-10	0.19	0.00
$3d^2 \ ^3F_4$	$3d4p \ ^3F_3$	1300.495	2.489E-03	3.174E-03	-27.54	3.75
$3d^2 \ ^3F_4$	$3d4p \ ^3F_4$	1313.853	3.893E-02	4.913E-02	-26.20	58.62
$3d^2 \ ^3F_4$	$3d4p \ ^3D_3$	1905.136	2.499E-02	2.372E-02	5.08	37.63
$3d^2 \ ^3F_4$	$3d4p \ ^1F_3$	3366.777	7.887E-08	8.891E-08	-12.74	0.00
$3d^2 \ ^3F_4$	$4s4f \ ^3F_3$	7476.468	8.641E-09	5.454E-08	-531.16	0.00
$3d^2 \ ^3F_4$	$4s4f \ ^3F_4$	7479.096	1.246E-07	7.938E-07	-537.00	0.00
$3d^2 \ ^3F_4$	$4s4f \ ^1F_3$	8587.377	1.090E-10	4.795E-10	-339.84	0.00
$4s5g \ ^3G_5$	$3d4p \ ^3F_4$	1113.838	5.774E-04	5.741E-04	0.57	1.13
$4s5g \ ^3G_5$	$4s4f \ ^3F_4$	3698.457	5.062E-02	4.824E-02	4.70	98.86
$4s5g \ ^3G_5$	$4s5f \ ^3F_4$	89493.467	4.431E-06	4.434E-06	-0.07	0.01
$4s5g \ ^1G_4$	$3d4p \ ^3F_3$	1104.089	4.806E-05	4.773E-05	0.69	0.07
$4s5g \ ^1G_4$	$3d4p \ ^3F_4$	1113.702	2.859E-06	2.823E-06	1.24	0.00
$4s5g \ ^1G_4$	$3d4p \ ^3D_3$	1511.298	7.408E-07	7.175E-07	3.14	0.00
$4s5g \ ^1G_4$	$3d4p \ ^1F_3$	2305.178	2.755E-02	2.658E-02	3.53	40.61
$4s5g \ ^1G_4$	$4s4f \ ^3F_3$	3696.325	3.928E-03	3.743E-03	4.69	5.79
$4s5g \ ^1G_4$	$4s4f \ ^3F_4$	3696.967	2.649E-04	2.523E-04	4.77	0.39
$4s5g \ ^1G_4$	$4s4f \ ^1F_3$	3948.886	3.606E-02	3.409E-02	5.45	53.14
$4s5g \ ^1G_4$	$4s5f \ ^3F_3$	88409.513	3.588E-07	3.594E-07	-0.17	0.00
$4s5g \ ^1G_4$	$4s5f \ ^3F_4$	88628.911	2.384E-08	2.424E-08	-1.68	0.00
$4s5g \ ^1G_4$	$4s5f \ ^1F_3$	140706.346	9.701E-07	2.417E-05	-2391.78	0.00

Table 7
Comparison of transition probabilities with literature values.

Final state	Initial state	This work ($L, 10^8 \text{ s}^{-1}$)	Other theory (10^8 s^{-1})	Diff.	NIST	Diff. (%)
4s4p 1P_1	4s 2 1S_0	2.170E+00	2.171E+00 MPCJ [9] 2.15E+00 CI+MBPT [11]	−0.02 0.9	2.18E+00	−0.44
4s4p 3P_1	4s 2 1S_0	2.738E−05	2.75E−05 CI+MBPT [11] 2.098E−05 MCHF [10]	0.43 23.37	2.6E−05	5.30
4s4p 1P_1	3d4s 1D_2	5.341E−05	5.274E−05 MPCJ [9] 5.70E−05 CI+MBPT [11]	1.26 6.72		
4s6f 1F_3	3d4s 1D_2	8.390E−02	8.570E−02 MPCJ [9]	−2.10	9.0E−01	−90.68
4s5p 1P_1	4s 2 1S_0	7.505E−03	5.850E−03 MPCJ [9]	28.30	2.7E−03	177.96
4s5p 1P_1	3d4s 1D_2	1.301E−01	1.440E−01 MPCJ [9]	−9.71	1.2E−01	8.38
4p 2 1D_2	4s4p 1P_1	5.760E−01	6.393E−01 MPCJ [9]	−9.90	6.6E−01	−12.73
4s6p 1P_1	4s 2 1S_0	9.182E−02	1.398E−01 MPCJ [9]	−34.33	1.67E−01	−45.02
4s6p 1P_1	3d4s 1D_2	2.379E−01	2.871E−01 MPCJ [9]	−17.14	3.3E−01	−27.91
4p 2 1S_0	4s4p 1P_1	7.780E−01	7.605E−01 MPCJ [9]	2.31	1.1E+00	−29.27
4s4f 1F_3	3d4s 1D_2	3.116E−01	2.622E−01 MPCJ [9]	18.82	1.88E−01	65.73
4s5d 1D_2	4s4p 1P_1	4.710E−01	3.930E−01 MPCJ [9]	19.83	4.0E−01	17.75
4snp 1P_1	4s 2 1S_0	3.246E−01	2.772E−01 MPCJ [9]	17.08	3.01E−01	7.84
4snp 1P_1	3d4s 1D_2	3.673E−01	2.801E−01 MPCJ [9]	31.13	4.1E−01	−10.42
4s5f 1F_3	3d4s 1D_2	1.884E−01	1.398E−01 MPCJ [9]	34.74	1.9E−01	−0.83
4s6d 1D_2	4s4p 1P_1	1.425E−01	8.248E−02 MPCJ [9]	72.76	8.0E−02	78.12
4s7p 1P_1	4s 2 1S_0	1.295E−01	1.546E−01 MPCJ [9]	16.23	1.53E−01	46.82
4s5s 1S_0	4s4p 1P_1	2.293E−01	2.401E−01 MPCJ [9]	−4.48		
4s6f 1F_3	4s4d 1D_2	5.391E−03	3.926E−03 MPCJ [9]	37.31		
4s6f 1F_3	4p 2 1D_2	2.969E−03	3.131E−03 MPCJ [9]	−5.16		
4s6f 1F_3	4s5d 1D_2	5.037E−03	4.493E−03 MPCJ [9]	12.09		
4s6f 1F_3	4s5g 1G_4	5.901E−03	7.346E−03 MPCJ [9]	−19.66		
4s5p 1P_1	4s5s 1S_0	2.361E−02	2.354E−02 MPCJ [9]	0.30		
4s4d 1D_2	3d4p 1D_2	2.778E−05	4.910E−05 MPCJ [9]	−43.43		
4s4d 1D_2	4s5p 1P_1	1.270E−04	1.395E−04 MPCJ [9]	−8.97		
4s4d 1D_2	4s4p 1P_1	1.601E−01	1.537E−01 MPCJ [9]	4.18		
3d4p 1F_3	4s4d 1D_2	1.565E−02	9.734E−03 MPCJ [9]	60.83		
3d4p 1F_3	3d4s 1D_2	5.705E−02	1.189E−01 MPCJ [9]	−52.01		
4s6s 1S_0	4s5p 1P_1	5.484E−02	4.506E−02 MPCJ [9]	21.72		
4s6s 1S_0	4s4p 1P_1	1.420E−02	4.357E−02 MPCJ [9]	−67.41		
4p 2 1D_2	3d4p 1D_2	2.401E−03	4.125E−03 MPCJ [9]	−41.78		
4p 2 1D_2	4s5p 1P_1	1.308E−02	1.228E−02 MPCJ [9]	6.55		
4p 2 1D_2	3d4p 1F_3	2.891E−07	2.208E−08 MPCJ [9]	92.39		
4s6p 1P_1	4s5s 1S_0	1.516E−02	2.310E−02 MPCJ [9]	−34.36		
4s6p 1P_1	4s4d 1D_2	1.407E−02	1.583E−02 MPCJ [9]	−11.12		
4s6p 1P_1	4s6s 1S_0	1.605E−03	1.313E−03 MPCJ [9]	22.30		
4s6p 1P_1	4p 2 1D_2	7.877E−04	6.613E−04 MPCJ [9]	19.11		
4p 2 1S_0	4s5p 1P_1	1.276E−02	2.607E−02 MPCJ [9]	−51.07		
4p 2 1S_0	4s6p 1P_1	2.055E−06	3.607E−07 MPCJ [9]	469.66		
4s4f 1F_3	4s4d 1D_2	6.368E−02	7.943E−02 MPCJ [9]	−19.83		
4s4f 1F_3	4p 2 1D_2	2.920E−03	2.743E−03 MPCJ [9]	6.46		
4s5d 1D_2	3d4p 1D_2	6.727E−04	8.300E−04 MPCJ [9]	−18.96		
4s5d 1D_2	4s5p 1P_1	3.302E−02	3.850E−02 MPCJ [9]	−14.25		
4s5d 1D_2	3d4p 1F_3	1.274E−03	1.029E−04 MPCJ [9]	91.92		
4s5d 1D_2	4s6p 1P_1	4.324E−03	3.961E−03 MPCJ [9]	9.15		
4s5d 1D_2	4s4f 1F_3	3.433E−04	3.752E−04 MPCJ [9]	−8.48		
4snp 1P_1	4s5s 1S_0	3.895E−02	3.431E−02 MPCJ [9]	13.55		
4snp 1P_1	4s4d 1D_2	1.273E−02	1.103E−02 MPCJ [9]	15.43		
4snp 1P_1	4s6s 1S_0	6.961E−03	8.416E−03 MPCJ [9]	−17.29		
4snp 1P_1	4p 2 1D_2	7.630E−04	5.603E−04 MPCJ [9]	36.19		
4snp 1P_1	4p 2 1S_0	3.175E−03	3.970E−03 MPCJ [9]	−20.04		
4snp 1P_1	4s5d 1D_2	2.552E−03	3.253E−03 MPCJ [9]	−21.56		
4s7s 1S_0	4s5p 1P_1	4.599E−02	3.338E−02 MPCJ [9]	37.80		
4s7s 1S_0	4s6p 1P_1	2.243E−02	1.532E−02 MPCJ [9]	46.47		
4s7s 1S_0	4snp 1P_1	3.074E−04	4.353E−04 MPCJ [9]	−29.39		
4s7s 1S_0	4s4p 1P_1	6.836E−02	8.625E−02 MPCJ [9]	20.74		
4s5f 1F_3	4s4d 1D_2	1.783E−02	1.474E−02 MPCJ [9]	20.91		
4s5f 1F_3	4p 2 1D_2	5.935E−03	3.063E−03 MPCJ [9]	93.77		
4s5f 1F_3	4s5d 1D_2	1.878E−02	1.853E−02 MPCJ [9]	1.35		
4s6d 1D_2	3d4p 1D_2	5.667E−05	3.354E−05 MPCJ [9]	68.96		
4s6d 1D_2	4s5p 1P_1	5.046E−02	3.690E−02 MPCJ [9]	36.75		
4s6d 1D_2	3d4p 1F_3	1.202E−03	1.296E−03 MPCJ [9]	−7.21		
4s6d 1D_2	4s6p 1P_1	7.402E−03	5.143E−03 MPCJ [9]	43.93		
4s6d 1D_2	4s4f 1F_3	3.857E−06	5.605E−06 MPCJ [9]	−31.18		
4s6d 1D_2	4snp 1P_1	2.409E−03	4.352E−03 MPCJ [9]	−44.65		
4s6d 1D_2	4s5f 1F_3	3.250E−05	5.590E−05 MPCJ [9]	−41.87		
4s7p 1P_1	4s5s 1S_0	1.135E−02	1.304E−02 MPCJ [9]	−12.95		
4s7p 1P_1	4s4d 1D_2	4.083E−03	4.259E−03 MPCJ [9]	−4.12		

(continued on next page)

Table 7 (continued)

Final state	Initial state	This work ($L, 10^8 \text{ s}^{-1}$)	Other theory (10^8 s^{-1})	Diff.	NIST	Diff. (%)
4s7p ¹ P ₁	4s6s ¹ S ₀	4.763E–03	5.618E–03 MPPI [9]	–15.22		
4s7p ¹ P ₁	4p ² ¹ D ₂	1.349E–03	1.127E–03 MPPI [9]	19.66		
4s7p ¹ P ₁	4s5d ¹ D ₂	7.689E–04	5.028E–05 MPPI [9]	93.46		
4s7p ¹ P ₁	4s7s ¹ S ₀	2.597E–03	5.038E–03 MPPI [9]	–48.46		
4s7p ¹ P ₁	4s6d ¹ D ₂	4.250E–04	8.985E–04 MPPI [9]	–52.70		
4s7p ¹ P ₁	3d4s ¹ D ₂	1.575E–01	1.118E–01 MPPI [9]	40.78		
4s8s ¹ S ₀	4s5p ¹ P ₁	1.964E–02	1.834E–02 MPPI [9]	7.10		
4s8s ¹ S ₀	4s6p ¹ P ₁	6.149E–03	8.316E–03 MPPI [9]	–26.06		
4s8s ¹ S ₀	4snp ¹ P ₁	7.344E–05	7.689E–04 MPPI [9]	–90.45		
4s8s ¹ S ₀	4s7p ¹ P ₁	2.071E–03	2.235E–03 MPPI [9]	–7.31		
4s8s ¹ S ₀	4s4p ¹ P ₁	3.569E–02	3.693E–02 MPPI [9]	–3.36		
3d4p ¹ D ₂	3d4s ³ D ₁	9.127E–02	6.680E–02 MCHF [10]	36.63	9.0E–02	1.41
3d4p ¹ D ₂	3d4s ³ D ₂	1.210E–02	9.061E–03 MCHF [10]	33.56	1.4E–02	–13.56
4s5s ¹ S ₀	4s4p ³ P ₁	1.694E–05	5.201E–06 MCHF [10]	225.74		
3d4p ³ F ₂	3d4s ¹ D ₂	1.267E–01	8.431E–02 MCHF [10]	50.30		
3d4p ³ F ₃	3d4s ¹ D ₂	5.039E–05	7.257E–05 MCHF [10]	–30.57		
3d4p ¹ D ₂	3d4s ³ D ₃	1.798E–03	7.160E–04 MCHF [10]	151.07		
4s5p ³ P ₁	4s ² ¹ S ₀	2.340E–06	4.098E–05 MCHF [10]	–94.28		
4s5p ³ P ₁	3d4s ¹ D ₂	1.051E–03	6.208E–04 MCHF [10]	69.35		
4s5p ³ P ₂	3d4s ¹ D ₂	1.792E–03	1.454E–04 MCHF [10]	91.88		
4s5p ¹ P ₁	3d4s ³ D ₂	2.354E–04	2.884E–04 MCHF [10]	–18.38		
4s4d ¹ D ₂	4s4p ³ P ₁	4.043E–06	1.222E–05 MCHF [10]	–66.92		
4s4d ¹ D ₂	4s4p ³ P ₂	2.657E–04	1.709E–04 MCHF [10]	55.50		
3d4s ¹ D ₂	4s4p ³ P ₂	8.245E–07	8.86E–07 CI+MBPT [11]	6.94		
4s5s ³ S ₁	4s4p ¹ P ₁	5.911E–06	6.13E–06 CI+MBPT [11]	3.59		
4s6d ³ D ₁	4s4p ³ P ₀	1.707E–01			1.51E–01	13.05
4s6d ³ D ₁	4s4p ³ P ₁	1.280E–01			1.11E–01	15.32
4s6d ³ D ₁	4s4p ³ P ₂	8.498E–03			5.9E–03	44.03
4s6d ³ D ₂	4s4p ³ P ₁	2.294E–01			1.78E–01	28.89
4s6d ³ D ₂	4s4p ³ P ₂	7.651E–02			6.5E–02	17.71
4s6d ³ D ₃	4s4p ³ P ₂	3.055E–01			2.23E–01	36.98
4s4d ³ D ₁	4s4p ³ P ₀	4.415E–01			4.98E–01	–11.35
4s4d ³ D ₁	4s4p ³ P ₁	3.223E–01			3.42E–01	–5.76
4s4d ³ D ₁	4s4p ³ P ₂	2.034E–02			2.45E–02	–16.96
4s4d ³ D ₂	4s4p ³ P ₁	5.939E–01			6.7E–01	–11.35
4s4d ³ D ₂	4s4p ³ P ₂	1.882E–01			2.0E–01	–5.92
4s4d ³ D ₃	4s4p ³ P ₂	7.793E–01			8.7E–01	–10.43
3d4p ³ D ₁	4s ² ¹ S ₀	7.250E–05			1.6E–04	–54.69
3d4p ³ D ₁	3d4s ³ D ₁	5.100E–01			4.3E–01	18.59
3d4p ³ D ₁	3d4s ³ D ₂	1.788E–01			1.4E–01	27.70
3d4p ³ D ₂	3d4s ³ D ₁	1.062E–01			8.3E–02	27.93
3d4p ³ D ₂	3d4s ³ D ₂	4.691E–01			3.8E–01	23.46
3d4p ³ D ₂	3d4s ³ D ₃	1.146E–01			8.6E–02	33.26
3d4p ³ D ₃	3d4s ³ D ₂	8.072E–02			6.0E–02	34.53
3d4p ³ D ₃	3d4s ³ D ₃	6.113E–01			4.9E–01	24.75
4p ² ³ P ₀	4s4p ³ P ₁	1.826E+00			1.99E+00	–8.24
4p ² ³ P ₁	4s4p ³ P ₀	6.116E–01			6.0E–01	1.93
4p ² ³ P ₁	4s4p ³ P ₁	4.633E–01			4.66E–01	–0.57
4p ² ³ P ₁	4s4p ³ P ₂	7.551E–01			7.4E–01	2.04
4p ² ³ P ₂	4s4p ³ P ₁	4.571E–01			4.34E–01	5.33
4p ² ³ P ₂	4s4p ³ P ₂	1.376E+00			1.36E+00	1.18
3d4p ³ P ₀	3d4s ³ D ₁	7.748E–01			6.0E–01	29.13
3d4p ³ P ₁	4s ² ¹ S ₀	8.447E–05			1.7E–04	–50.31
3d4p ³ P ₁	3d4s ³ D ₁	2.025E–01			1.5E–01	35.03
3d4p ³ P ₁	3d4s ³ D ₂	5.712E–01			4.4E–01	29.82
3d4p ³ P ₂	3d4s ³ D ₁	8.820E–03			6.1E–03	44.59
3d4p ³ P ₂	3d4s ³ D ₂	1.248E–01			9.1E–02	37.10
3d4p ³ P ₂	3d4s ³ D ₃	6.382E–01			5.0E–01	27.63
4s6s ³ S ₁	4s4p ³ P ₀	2.621E–02			3.34E–02	–21.53
4s6s ³ S ₁	4s4p ³ P ₁	7.994E–02			9.8E–02	–18.43
4s6s ³ S ₁	4s4p ³ P ₂	1.377E–01			1.75E–01	–21.34
4s6f ³ F ₂	3d ² ³ F ₃	5.931E–02			7.2E–02	–17.63
4s6f ³ F ₂	4s7s ³ S ₁	1.101E–02			9.8E–03	12.34
4s6f ³ F ₂	3d4s ³ D ₃	3.166E–04			3.5E–04	–9.56
4s6f ³ F ₃	4s6d ¹ D ₂	6.277E–02			5.4E–02	16.23
4s6f ³ F ₃	3d4s ³ D ₃	7.898E–03			8.9E–03	–11.26
4s6f ³ F ₄	3d4s ³ D ₃	7.088E–02			7.9E–02	–10.28
4s8s ³ S ₁	4s4p ³ P ₀	7.436E–03			9.4E–03	–20.90
4s8s ³ S ₁	4s4p ³ P ₁	2.225E–02			3.0E–02	–25.83
4s8s ³ S ₁	4s4p ³ P ₂	3.693E–02			5.3E–02	–30.33
4s5f ³ F ₂	3d4s ³ D ₁	1.106E–01			1.1E–01	0.52
4s5f ³ F ₂	3d4s ³ D ₂	2.057E–02			2.1E–02	–2.05

(continued on next page)

Table 7 (continued)

Final state	Initial state	This work ($L, 10^8 \text{ s}^{-1}$)	Other theory (10^8 s^{-1})	Diff.	NIST	Diff. (%)
4s5f 3F_2	3d4s 3D_3	5.884E-04			5.8E-04	1.45
4s5f 3F_3	3d4s 3D_2	1.172E-01			1.2E-01	-2.36
4s5f 3F_3	3d4s 3D_3	1.471E-02			1.5E-02	-1.97
4s5f 3F_4	3d4s 3D_3	1.323E-01			1.3E-01	1.79
4s7s 3S_1	4s4p 3P_0	1.873E-02			1.3E-02	44.07
4s7s 3S_1	4s4p 3P_1	5.630E-02			4.6E-02	22.38
4s7s 3S_1	4s4p 3P_2	9.417E-02			7.8E-02	20.73
4s5d 3D_1	4s4p 3P_0	1.927E-01			2.12E-01	-9.12
4s5d 3D_1	4s4p 3P_1	1.452E-01			1.53E-01	-5.10
4s5d 3D_1	4s4p 3P_2	9.773E-03			9.5E-03	2.87
4s5d 3D_2	4s4p 3P_1	2.593E-01			2.97E-01	-12.69
4s5d 3D_2	4s4p 3P_2	8.734E-02			9.4E-02	-7.08
4s5d 3D_3	4s4p 3P_2	3.451E-01			3.55E-01	-2.78
4s4f 3F_2	3d4s 3D_1	1.348E-01			1.76E-01	-23.43
4s4f 3F_2	3d4s 3D_2	2.508E-02			3.5E-02	-28.33
4s4f 3F_2	3d4s 3D_3	7.142E-04			9.8E-04	-27.13
4s4f 3F_3	3d4s 3D_2	1.429E-01			2.09E-01	-31.63
4s4f 3F_3	3d4s 3D_3	1.791E-02			2.5E-02	-28.38
4s4f 3F_4	3d4s 3D_3	1.617E-01			2.29E-01	-29.40
4s5p 3P_2	3d4s 3D_1	6.273E-04			2.3E-03	-72.72
4s5p 3P_2	3d4s 3D_2	1.558E-02			3.3E-02	-52.79
4s5p 3P_2	3d4s 3D_3	8.710E-02			1.9E-01	-54.16
4s5p 3P_1	3d4s 3D_1	2.532E-02			5.6E-02	-54.79
4s5p 3P_1	3d4s 3D_2	7.859E-02			1.7E-01	-53.77
3d4p 3F_4	3d4s 3D_3	3.850E-01			5.3E-01	-27.36
4s5p 3P_0	3d4s 3D_1	1.045E-01			2.2E-01	-52.48
3d4p 3F_3	3d4s 3D_2	3.367E-01			4.7E-01	-28.36
3d4p 3F_3	3d4s 3D_3	4.447E-02			5.9E-02	-24.62
3d4p 3F_2	3d4s 3D_1	2.250E-01			4.4E-01	-48.86
3d4p 3F_2	3d4s 3D_2	4.840E-02			8.1E-02	-40.25
3d4p 3F_2	3d4s 3D_3	7.591E-04			2.4E-03	-68.37
4s5s 3S_1	4s4p 3P_0	9.246E-02			9.6E-02	-3.69
4s5s 3S_1	4s4p 3P_1	2.759E-01			2.87E-01	-3.88
4s5s 3S_1	4s4p 3P_2	4.549E-01			4.77E-01	-4.63